RELAP-7 User's Guide

Hongbin Zhang, Haihua Zhao, Ling Zou, David Andrs, Ray Berry, Richard **Martineau**

December 2014

U.S. Department of Energy Office of Nuclear Energy

DISCLAIMER

This information was prepared as an account of work sponsored by an agency of the U.S. Government. Neither the U.S. Government nor any agency thereof, nor any of their employees, makes any warranty, expressed or implied, or assumes any legal liability or responsibility for the accuracy, completeness, or usefulness, of any information, apparatus, product, or process disclosed, or represents that its use would not infringe privately owned rights. References herein to any specific commercial product, process, or service by trade name, trade mark, manufacturer, or otherwise, does not necessarily constitute or imply its endorsement, recommendation, or favoring by the U.S. Government or any agency thereof. The views and opinions of authors expressed herein do not necessarily state or reflect those of the U.S. Government or any agency thereof.

RELAP-7 User's Guide

Hongbin Zhang, Haihua Zhao, Ling Zou, David Andrs, Ray Berry, Richard Martineau

December 2014

Idaho National Laboratory Idaho Falls, Idaho 83415

http://www.inl.gov

Prepared for the U.S. Department of Energy Office of Nuclear Energy Under DOE Idaho Operations Office Contract DE-AC07-05ID14517

Contents

Figures

Tables

RELAP-7 Overview

The RELAP-7 code is the next generation nuclear reactor system safety analysis code being developed at the Idaho National Laboratory (INL). The code is based on the INL's modern scientific software development framework, MOOSE (Multi-Physics Object Oriented Simulation Environment). The overall design goal of RELAP-7 is to take advantage of the previous thirty years of advancements in computer architecture, software design, numerical integration methods, and physical models. The end result will be a reactor systems analysis capability that retains and improves upon RELAP5's capability and extends the analysis capability for all reactor system simulation scenarios.

RELAP-7 will become the main reactor systems simulation toolkit for the LWRS (Light Water Reactor Sustainability) program's RISMC (Risk Informed Safety Margin Characterization) effort and the next generation tool in the RELAP reactor safety/systems analysis application series. The key to the success of RELAP-7 is the simultaneous advancement of physical models, numerical methods, and software design while maintaining a solid user perspective. Physical models include both PDEs (Partial Differential Equations) and ODEs (Ordinary Differential Equations) and experimental based closure models. RELAP-7 utilizes well-posed governing equations for compressible two-phase flow, which can be strictly verified in a modern verification and validation effort. Closure models used in RELAP5 and newly developed models will be reviewed and selected to reflect the progress made during the past three decades and provide a basis for the closure relations that will be required in RELAP-7. RELAP-7 uses modern numerical methods, which allow implicit time integration, second-order schemes in both time and space, and strongly coupled multi-physics.

RELAP-7 is written with object oriented programming language C++. By using the MOOSE development environment, the RELAP-7 code is developed by following the same modern software design paradigms used for other MOOSE development efforts. The code is easy to read, develop, maintain, and couple with other codes. Most importantly, the modern software design allows the RELAP-7 code to evolve efficiently with time. MOOSE is an HPC development and runtime framework for solving computational engineering problems in a well planned, managed, and coordinated way. By leveraging millions of lines of open source software packages, such as PETSc (a nonlinear solver developed at Argonne National Laboratory) and LibMesh (a Finite Element Analysis package developed at University of Texas), MOOSE reduces the expense and time required to develop new applications. MOOSE provides numerical integration methods and mesh management for parallel computation. Therefore RELAP-7 code developers have been

able to focus more upon the physics and user interface capability. There are currently over 20 different MOOSE based applications ranging from 3-D transient neutron transport, detailed 3-D transient fuel performance analysis, to long-term material aging. Multiphysics and multi-dimensional analysis capabilities, such as radiation transport and fuel performance, can be obtained by coupling RELAP-7 and other MOOSE-based applications through MOOSE and by leveraging with capabilities developed by other DOE programs. This allows restricting the focus of RELAP-7 to systems analysis type simulations and gives priority to retain and significantly extend RELAP5's capabilities.

This document provides a user's guide to help users to learn how to run the RELAP-7 code. A number of example problems and their associated input files are presented in this document to guide users to run the RELAP-7 code starting with simple pipe problems to problems with increasing complexity. Because the code is an ongoing development effort, this RELAP-7 User's Guide will evolve with periodic updates to keep it current with the state of the development, implementation, and model additions/revisions. A complete User's Manual will be developed at a later time when the RELAP-7 code becomes more mature.

1 RELAP-7 Features

An overall description of the RELAP-7 architecture, governing theory, and computational approach is given here as an instructive, and executive overview of the RELAP-7 distinguishing features.

1.1 Software Framework

MOOSE is INL's development and runtime environment for the solution of multi-physics systems that involve multiple physical models or multiple simultaneous physical phenomena. The systems are generally represented (modeled) as a system of fully coupled nonlinear partial differential equation systems (an example of a multi-physics system is the thermal feedback effect upon neutronics cross-sections where the cross-sections are a function of the heat transfer). Inside MOOSE, the Jacobian-Free Newton Krylov (JFNK) method [\[1,](#page-152-1) [2\]](#page-152-2) is implemented as a parallel nonlinear solver that naturally supports effective coupling between physics equation systems (or Kernels). The physics Kernels are designed to contribute to the nonlinear residual, which is then minimized inside of MOOSE. MOOSE provides a comprehensive set of finite element support capabilities (LibMesh [\[3\]](#page-152-3), a Finite Element library developed at University of Texas) and provides for mesh adaptation and parallel execution. The framework heavily leverages software libraries from DOE SC and NNSA, such as the nonlinear solver capabilities in either the the Portable, Extensible Toolkit for Scientific Computation (PETSc [\[4\]](#page-152-4)) project or the Trilinos project [\[5\]](#page-152-5) (a collection of numerical methods libraries developed at Sandia National Laboratory). Argonne's PETSc group has recently joined with the MOOSE team in a strong collaboration wherein they are customizing PETSc for our needs. This collaboration is strong enough that Argonne is viewed as a joint developer of MOOSE.

A parallel and tightly coordinated development effort with the RELAP-7 development project is the Reactor Analysis Virtual control ENvironment (RAVEN). This MOOSEbased application is a complex, multi-role software tool that will have several diverse tasks including serving as the RELAP-7 graphical user interface, using RELAP-7 to perform RISMC focused analysis, and controlling the RELAP-7 calculation execution.

Together, MOOSE/RELAP-7/RAVEN comprise the systems analysis capability of LWRS RISMC ToolKit.

1.2 Governing Theory

The primary basis of the RELAP-7 governing theory includes thermal fluids flow, reactor core heat transfer, and reactor kinetics models.

With respect to the thermal fluids flow dynamics models, RELAP-7 incorporates both single- and two-phase flow simulation capabilities encompassing all-speed and all-fluids. The single phase flow models include isothermal flow and nonisotherml flow capabilities. The two-phase flow models include the homogeneous equilibrium flow model (HEM) and the well posed two fluid 7-equation model.

In addition to the fluids flow dynamics model, RELAP-7 necessarily simulates the heat transfer process with reactor kinetics as the heat source. The heat-conduction equation for cylindrical or slab geometries is solved to provide thermal history within metal structures such as fuel and clad. The volumetric power source in the heat conduction equation for the fuel comes from the point kinetics model with thermal hydraulic reactivity feedback considered [\[6\]](#page-152-6). The reactor structure is coupled with the thermal fluid through energy exchange (conjugate heat transfer) employing surface convective heat transfer [\[7\]](#page-152-7) within the fluid . The fluid, heat conduction, conjugate heat transfer and point kinetics equations are solved in a fully coupled fashion in RELAP-7 in contrast to the operator-splitting or loose coupling approach used in the existing system safety analysis codes.

1.3 Computational Approach

Stated previously, the MOOSE framework provides the bulk of the "heavy lifting" available to MOOSE-based applications with a multitude of mathematical and numerical libraries. For RELAP-7, LibMesh [\[3\]](#page-152-3) provides the second-order accurate spatial discretization by employing linear basis, one-dimensional finite elements. The Message Passing Interface (MPI, from Argonne National Laboratory) provides for distributed parallel processing. Intel Threading Building Blocks (Intel TBB) allows parallel C++ programs to take full advantage of multicore architecture found in most large-scale machines of today. PETSc (from Argonne), Trilinos (from Sandia), and Hypre [\[8\]](#page-152-8) (from Lawrence Livermore National Laboratory) provide the mathematical libraries and nonlinear solver capabilities for the Jacobian-free Newton-Krylov (JFNK) method. In MOOSE, a stiffly-stable, secondorder backward difference (BDF2) formulation is used to provide second-order accurate time integration for strongly coupled physics in JFNK.

The JFNK method easily allows implicit nonlinear coupling of dependent physics under one general computational framework. Besides rapid (second-order) convergence of the iterative procedure, the JFNK method flexibly handles multiphysics problems when time scales of different physics are significantly varied during transients. The key feature of the JFNK method is combining Newton's method to solve implicit nonlinear systems with Krylov subspace iterative methods. The Krylov methods do not require an explicit form of the Jacobian, which eliminates the computationally expensive step of forming Jacobian matrices (which also may be quite difficult to determine analytically), required by Newton's method. The matrix-vector product can be approximated by the numerical differentiation of nonlinear residual functions. Therefore, JFNK readily integrates different physics into one solver framework.

2 Model Description

2.1 Fluids Flow Models

The RELAP-7 code has various flow models implemented. These include:

- 1). a single phase isothermal flow model (model_type=2),
- 2). a single phase nonisothermal fluid flow model $(mod \ell$.
- 3). a homogeneous equilibrium (HEM) two phase flow model (model type=32),

4). a nonhomogeneous, nonequilibrium seven-equation two phase flow model $(\text{model-type}=7)$.

2.2 Equation of State

For the single phase flow models, various types of equation of state can be used. These include:

1). Barotropic equation of state for isothermal flow. This is turned on by setting type=BarotropicEquationOfState.

2). Linear equation of state for non-isothermal single phase flow. This is turned on by setting type = NonIsothermalEquationOfState.

3). Stiffened gas equation of state which is turned on by setting

type = StiffenedGasEquationOfStateVapor for single phase vapor flow and

type = StiffenedGasEquationOfStateLiquid for single phase water flow.

4). Ideal gas equation of state which is turned on by setting type=IdealGasEquationOfState. The equation of state for the nitrogen gas has also been implemented into the code. It can be turned on by setting type=N2Properties.

For the **homogeneous equilibrium flow model**, only the stiffened gas equation of state is applicable. This is turned on by setting type = TwoPhaseStiffenedGasEOS.

For the seven-equation two phase flow model, only the stiffened gas equation of state is applicable. This is turned on by setting

```
type = StiffenedGasEquationOfStateLiquid for the liquid phase,
and type = StiffenedGasEquationOfStateVapor for the vapor phase.
```
2.3 Solution Stabilization Schemes

It is well known that the continuous Galerkin finite element method is unstable when applied directly to hyperbolic systems of equations. Therefore the solution stabilization schemes are required for RELAP-7. Currently available options of solution stabilization for RELAP-7 include:

1). Streamline Upwind/Petrov Galerkin method (SUPG). The SUPG scheme works for the single phase flow only. It can be used by setting stabilization_type = 'SUPG'.

2). Lapidus scheme works for both the single phase flow and the two phase flow cases. It can be used by setting stabilization type = $'$ LAPIDUS'.

3). The entropy viscosity method works for both the single phase flow and the two phase flow. This option can be used by setting stabilization_type = 'ENTROPY_VISCOSITY'.

2.4 Time Integration Schemes

There are two types of time integration schemes in RELAP-7 - Implicit Euler and BDF2. Implicit Euler is a first order accurate time integration scheme. This can be turned on by setting:scheme = 'implicit-euler' in the Executioner input block (explained later). BDF2 is a second order accurate time integration scheme. This is the default option for RELAP-7.

2.5 Components

A real reactor system is very complex and contains hundreds of different physical components. It is impractical to resolve the real geometry of the entire system. Instead simplified thermal hydraulic models are used to represent (via "nodalization") the major physical components and describe the major physical processes (such as fluids flow and heat transfer). There are three main types of components developed in RELAP-7: (1) onedimensional (1-D) components describing the geometry of the reactor system, (2) zerodimensional (0-D) components for setting boundary conditions, and (3) 0-D components for connecting 1-D components.

2.5.1 Pipe

Pipe is the most basic component in RELAP-7. It is a 1-D component which simulates thermal fluids flow in a pipe. Both a constant cross section area and a variable cross section area options are available for the Pipe component. The wall friction and heat transfer coefficients are either calculated through closure models or provided by user input. The pipe wall temperature can be provided as the wall heat transfer boundary condition. All the thermal fluids dynamic models are available in the Pipe component which includes the isothermal flow model, single-phase non-isothermal flow model, nonequilibrium 7 equation two-phase model, and the much simpler homogeneous equilibrium two-phase flow model.

2.5.2 PipeWithHeatStructure

The PipeWithHeatStructure component simulates fluids flow in a 1-D pipe coupled with 1-D or 2-D heat conduction through the pipe wall. The adiabatic, Dirichlet, or convective boundary conditions at the outer surface of the pipe wall are available. Either a plate type or cylindrical type of heat structure can be selected. Volumetric heat source within the fluids or solid materials can be added.

2.5.3 CoreChannel

The CoreChannel component is a composite component designed to simulate the coolant flow and heat conduction inside a fuel rod as well as the conjugate heat transfer between the coolant and the fuel rod. In this component, the fuel rod is divided into the same number of segments as that of the coolant flow pipe elements. Each fuel rod segment is further simulated as 1-D or 2-D heat conduction model perpendicular to the fluid flow model. Both plate type fuel rod and cylindrical fuel rod type can be simulated. The solid fuel part is able to deal with typical LWR fuel rod with complex clad/gap/fuel pellet geometries. The flow model and conjugate heat transfer model are fully coupled in contrast to loosely coupled in RELAP5.

2.5.4 Subchannel

A fully coupled subchannel channel model for the single-phase has been implemented into RELAP-7. The single-phase subchannel model includes four balance equations: mass, energy, axial momentum, and lateral momentum.

2.5.5 HeatExchanger

A Heat Exchanger component is a combination of two pipes with a solid wall in between. Similar to the CoreChannel model, the fluids flow model and conjugate heat transfer model are fully coupled. More complicated and realistic steam generator component will be developed in the future.

2.5.6 Branch

The branch model is a 0-D component representing a junction model with no volume (inertia) effects considered, and with single/multiple inlets and single/multiple outlets, of which cross section areas can be different. This model conserves the mass and energy among all connecting components.

2.5.7 VolumeBranch

The volume branch model is a 0-D component representing a joint/junction model with volume (inertia) effects considered. This model conserves the mass and energy among all connecting components.

2.5.8 SubchannelBranch

This is a 0D branch model to connect the subchannel component.

2.5.9 Pump

A simple pump model to provide a head and a reverse flow form loss coefficient (*K*) for either isothermal flow and non-isothermal flow. It can be driven by an user input head or through a driving component which provides shaft work.

2.5.10 Turbine

The turbine model in RELAP-7 is a simplified dynamical turbine model to simulate a reactor core isolation cooling (RCIC) turbine, which drives the RCIC pump through a common shaft.

2.5.11 SeparatorDryer

The separator dryer model in RELAP-7 separates steam and water with mechanical methods. Only an ideal separator dryer model is available in RELAP-7.

2.5.12 DownComer

The down comer component simulates a large volume to mix different streams of water and steam and to track the water level.

2.5.13 Valve

The valve component simulates the open and close behaviors of valves for incompressible flow with user given trigger and response time. The abrupt area change model is used to calculate the form loss.

2.5.14 CompressibleValve

The compressible valve component simulates the open and close behavior of valves for compressible fluid flow, including ckoking. It can be used to simulate the safety relief valves (SRV) of BWRs.

2.5.15 Check Valves

The check valve component simulates the dynamic behavior of check valves, with the form loss calculated by the abrupt area change model.

2.5.16 WetWell

The wet well component simulates the dynamic response of a BWR suppression pool and its gas space.

2.5.17 TimeDependentVolume

The time depedent volume component provides pressure, temperature, and void fraction boundary conditions as constants or time dependent functions for 1-D components. It is a pure boundary condition type of component and it does not add any entries to the global unknown vector. When acquired by its connected 1-D component, it provides a pressure, a temperature, and a void fraction boundary condition.

2.5.18 TimeDependentJunction

The time dependent junction component provides velocity and temperature boundary conditions as constants or time functions for 1-D components.

2.5.19 Tdm

Tdm sets time dependent mass flow boundary conditions for 1-D components.

2.5.20 Reactor

A virtual component that allows users to input the power for the core channel component.

2.5.21 PointKinetics

The point kinetics model is a lumped parameter neutron kinetics model to calculate the reactor power. User input reactivity or fully coupled feedback reactivity models are available.

3 Running RELAP-7

3.1 Complete Step 1 of MOOSE Environment Setup

The system environment setup for MOOSE can be found with the link: <http://www.mooseframework.org/getting-started>

3.2 Setup Your SSH Key

SSH key allows you to establish a secure connection between your computer and GitLab. Before generating an SSH key, check to see if your system already has one by running cat /.ssh/id_rsa.pub. If you see a long string starting with ssh-rsa or ssh-dsa, you can skip the ssh-keygen step below.

To generate a new SSH key, just open your terminal and use the code below. The ssh-keygen command prompts you for a location and filename to store the key pair and for a password. When prompted for the location and filename you can press enter to use the default. It is a best practice to use a password for an SSH key but it is not required and you can skip creating a password by pressing enter. Note that the password you choose here can not be altered or retrieved.

ssh-keygen -t rsa -C "\$your email"

Use the code below to show your public key.

```
cat ∼/. ssh / id_rsa . pub
```
Copy and paste the key to the My SSH Key section under the SSH tab in your profile. Please copy the complete key starting with ssh- and ending with your username and host.

To test your SSH key.

```
$ssh git@hpcgitlab . inl . gov
Welcome to GitLab, <your name here>!
Connection to hpcgitlab. inl.gov closed.
```
3.3 Checking Out the Code

```
$ cd ∼/ projects /
$ git clone git@hpcgitlab . inl . gov : idaholab / relap -7. git
$ cd relap -7
$ git submodule update -- init
```
It is necessary to build libmesh before building any application.

```
$ cd ∼/ projects / relap -7/ moose
$ ./ update_and_rebuild_libmesh . sh
```
Once libmesh has been successfully compiled, you may now compile RELAP-7.

```
cd ∼/ projects / trunk / relap -7
make ( add -jn to run on multiple "n" processors )
```
Once RELAP-7 has been compiled successfully, it is recommended to run the tests to make sure the version of the code you have is running correctly.

```
cd ∼/ projects / trunk / relap -7
./ run_tests ( add -jn to run "n" jobs at one time )
```
3.4 Executing RELAP-7

When first starting out with running RELAP-7, it is recommended to start from an example problem. Multiple example problems with input files are presented in this document. More examples can be found under the /relap-7/tests subdirectory. To demonstrate how to run RELAP-7, consider the PWR core channel.i test problem.

```
cd ∼/ projects / trunk / relap -7/ examples / components / core_channel /
# To run with one processor
∼/ projects / trunk / relap -7/ relap -7 - opt -i PWR_core_channel .i
# To run in parallel (4 processors )
mpiexec -n 4 ../../../ relap -7 - opt -i PWR_core_channel .i
```
3.5 Post Processing

RELAP-7 typically writes solution data to an ExodusII file. The solution data may also be written in other formats, one being a comma separated values (CSV) file, which allows the solutionn data to be saved in a table structured format. The other being a tecplot file in either binary or ASCII format.

Several options exist for viewing ExodusII output files. One good choice is to use open-source software, Paraview (<www.paraview.org>).

3.6 Graphical User Interface

Another MOOSE based application named RAVEN provides a graphical user interface (GUI) for RELAP-7. RAVEN can be used to generate a text input fie. It is also capable of submitting the analysis and provides post processing capabilitis.

4 Input Files

RELAP-7 uses a block-structured input file. Each block is identified with square brackets. The opening brackets contain the type of the input block and the empty brackets mark the end of the block. Each block may contain subblocks.

```
[ BlockName ]
   < block line commands >
   [./ subblock_name ]
       < subblock line commands >
   [\cdot,\cdot/][]
```
Each subblock must have an unique name when compared with all other subblocks in the current block.

Line commands are given as parameter and value pairs with an equal sign between them. They specify parameters to be used by the object being described. The parameter is a string, and the value may be a string, an integer, a real number, or a list of strings, integers, or real numbers. Lists are given in single quotes and are separated by whitespace.

Subblocks normally contain a type line command. This line command specifies the particular type of object being described.

RELAP-7 uses SI units. This stsndardizes the model input by eliminating the possibility of errors caused by using one set of units for one model and another set of units for a different model.

The following subsections have brief descriptions of each block. More detailed descriptions can be found in the examples section.

4.1 Global Parameters

The GlobalParams block specifies the global parameters used by the code such as the initial pressure (global_init_P), velocity (global_init_V) and temperature (global_init_T) of the system model, the fluid flow model type $(model_type)$, the stabilzation scheme type (stabilization type), and the scaling factors (scaling factor var) for the primary variable, etc. The values of of global parameters are available to any other block or subblock in the input file. If a command line is missing in a block or a subblock but defined in GlobalParams, the block or subblock will use the parameter defined in GlobalParams. However, if the block or subblock has a command line , that will be used regardless of what is in GlobalParams.

The following is an example of the GlobalParams block:

```
[ GlobalParams ]
 global_init_P = 155. e5
 global_init_V = 0.
 global\_init_T = 559.15
 # model_type = 2
 # model_type = 32
 # model_type = 7
 model type = 3stabilization_type = 'SUPG '
 scaling_factor\_var = '1e4 1e1 1e-2'temperature_sf = '1e -2 '
[]
```
symbol indicates comments in the input file and can be located anywhere in the input file.

4.2 Equation of State

The EoS block specifies the equation of state to be used by the code. The following is an example of the EoS block:

```
[ EoS ]
  [./ eos ]
    type = NonIsothermalEquationOfState
    p_0 = 155.e5rho_0 = 686.
    a2 = 1.e7beta = .46e - 3cv = 5.5 e3e_0 = 3075325
    T_0 = 559.15[\ldots]
```
4.3 Materials

The Materials block specifies the properties of the solid materials for the code. The following is an example of the Materials block:

```
[ Materials ]
 [./fuel-mat]
   type = SolidMaterialProperties
    k = 2.5Cp = 300.
    rho = 1.032e4[\ldots][./ gap -mat]type = SolidMaterialProperties
    k = 0.6Cp = 1.
    rho = 1.
  [\ldots][./clad-mat]
    type = SolidMaterialProperties
   k = 21.5Cp = 350.rho = 6.55e3[\ldots][]
```
4.4 Functions

The Functions block provides the functions to be used by the code during the simulations such as reactor power as a function of time or a boundary condition pressure as a function of time, etc. The following is an example of defining pressure distribution as a function of x.

```
[ Functions ]
```
[]

```
[./p_func]axis = 0type = PiecewiseLinear
   x = '0 3'
   y = '1.05e5 1e5'
 [\ldots][]
```
4.5 Components

The Components block specifies the components to be used in the simulations.

```
[ Components ]
 [./reactor]
   type = Reactor
   initial_power = 77337.69407
  [\cdot,\cdot/][./ CCH1 ]
   type = CoreChannel
   eos = eos
    position = '0 0 0'orientation = '0 0 1'
    A = 8.7878e-5Dh = 0.01179
   length = 4n_elems = 20
    f = 0.01Hw = 5.33e4Phf = 0.029832559676
    Ts\_init = 559.15dim hs = 1fuel_type = cylinder
    name_of_hs = ' fuel gap clad '
    n_heatstruct = 3
    width_of_hs = '0.004096 0.0001 0.000552 '
    elem_number_of_hs = '10 1 2'
    material_hs = 'fuel-mat gap-mat clad-mat'
    power_fraction = '1.0 0.0 0.0 '
```

```
[\ldots][./ inlet ]
    type = TimeDependentVolume
    input = 'CCH1 (in)'p bc = 155.483 e5
    T_{bc} = 559.15eos = eos
  [\ldots][./ outlet ]
    type = TimeDependentVolume
    input = 'CCH1(out)'p_bc = '155.e5'T_{bc} = 559.15eos = eos
  [\ldots][]
```
4.6 Preconditioner

The Preconditioning block specifies the preconditioner to be used by the preconditioned JFNK solver for the RELAP-7 code. The solution algorithm for RELAP-7 is the Jacobian-free Newton-Krylov (JFNK) method. However the Krylov methods need preconditioning to be efficient. Hence, the solvers available in RELAP-7 are preconditioned JFNK (PJFNK). Two options are available in RELAP-7 to build the preconditioning matrix, the single matrix preconditioner (SMP) and the finite difference preconditioner (FDP). The SMP option uses all the Jacobian terms derived analytically to build one preconditioning matrix. The FDP option uses numerical Jacobian by doing direct finite differences of the residual terms. The SMP option is the more efficient and is the recommended option, while the FDP option is normally slow and inefficient and is recommended to be used for small problems or for debugging purposes. The following is an example of the Preconditioning block:

```
[ Preconditioning ]
  # Uncomment one of the lines below to activate one of the blocks...
   active = ' SMP_PJFNK '
  # active = ' FDP_PJFNK '
```

```
# The definitions of the above - named blocks follow .
  [./ SMP_PJFNK ]
   type = SMP
   full = true # off diagonal blocks are used
    solve_type = 'PJFNK ' # Preconditioned JFNK solver
  [\ldots][./ FDP_PJFNK ]
   type = FDP
    full = true
    solve_type = 'PJFNK '
  [\ldots][]
```
4.7 Executioner

The Executioner block specifies the executioner that will be used in the simulations. The options include Transient, RavenExecutioner, etc.

```
[ Executioner ]
 type = Transient
 dt = 0.5dtmin = 1.e-5petsc_options_iname = '- mat_fd_type - mat_mffd_type -pc_type '
 petsc_options_value = ' ds ds ds lu'
 nl_{rel\_tol} = 1e-8nl_abs\_tol = 1e-8nl_max\_its = 101_{\text{tol}} = 1e-41 max its = 60
  start_time = 0.0
 num_steps = 30
  [./ Quadrature ]
   type = TRAP
   order = FIRST
  [\ldots][]
```
4.8 Outputs

The Outputs block controls the various screen and file output in the simulations.

```
[ Outputs ]
 [./ out ]
   type = Exodus
   use_displaced = true
   output_initial = true
    sequence = false
    append_displaced = true
 [\ldots][./ console ]
   type = Console
   perf_log = true
  [../]
[ ]
```
5 Examples

5.1 Example 1: A Simple Pipe Flow Problem

5.1.1 Problem Description

Figure 1. A simple pipe flow problem diagram

Example 1 simulates water flowing through a pipe under isothermal conditions with the following parameters:

Hydraulic Diameter = .01 m Cross section flow area = $7.85e-5 m^2$ Length $= 1$ m Wall friction coefficient $= .01$

The boundary conditions are the following:

Inlet: Pressure $= 1.05e5$ Pa Outlet: Pressure = 1e5 Pa

A 1D model can be viewed in Paraview to visualize the process better. Once Paraview is opened, on the left, select all of the variables and click "Apply." In the filters tab, under "Data Analysis", select "Plot Over Line" and apply. When this is done, each parameter in the problem can be viewed plotted over the length of the pipe. The figure below shows pressure vs length.

Figure 2. Pressure vs. length for the simple pipe flow problem

The pressure difference can be hand calculated to check the code calculated results using:

$$
\Delta P = \frac{f L \rho u^2}{2D_h} \tag{1}
$$

Where ρ is the density and u is the velocity. Both values can be found in Paraview to perform the calculation.

5.1.2 Input File

The following shows the input file to run this example problem:

```
#
# Isothermal flow through one simple pipe with B.C. set by TDVs
#
[GlobalParams]
 model_type = 2scaling_factor_var = '1e+0 1e-4'
 stabilization_type = 'SUPG'
[][EoS]
 [./eos]
   type = BarotropicEquationOfState
   p_0 = 1.e5rho_0 = 1.e3a2 = 1.e7[\ldots][][Components]
 [./pipe1]
   type = Pipe
   eos = eos
   position = '000'orientation = '1 0 0'
   Dh = 0.01length = 1.0n_elems = 10
   A = 7.854e-5f = 0.01[\ldots][./inlet]
   type = TimeDependentVolume
   input = 'pipe1(in)'p_{bc} = 105e3eos = eos
 [\ldots]
```

```
[./outlet]
    type = TimeDependentVolume
    input = 'pipe1(out)'
   p\_bc = 1e5eos = eos
 [\ldots][[Preconditioning]
  [./SMP_PJFNK]
   type = SMP
   full = true
   solve_type = 'PJFNK'
 [\ldots][]
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1.25e-2dtmin = 1.e-5nl_rel_tol = 1e-8
 nl\_abs\_tol = 1e-6nl_max_its = 15
  l\_tol = 1e-6l_max\_its = 30start_time = 0.0
  end \times time = 250.0
 num_steps = 500
  [./Quadrature]
   type = TRAP
   order = FIRST
  [\ldots]
```
```
[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\ldots][./console]
   type = Console
   perf_log = true
  [../]
[]
```
[]

5.1.3 Description of the Input File

The following are the destailed descriptions of the input file block by block.

The Global Parameters block:

```
[ GlobalParams ]
 model\_type = 2scaling_factor\_var = '1e+0 1e-4'stabilization_type = 'SUPG '
[]
```


The Equation of State block:

```
[ EoS ]
  [./ eos ]
    type = BarotropicEquationOfState
    p_0 = 1.e5rho_0 = 1.e3a2 = 1.e7[\ldots][]
```
[./eos] Subblock for eos

- type The type of equation of state to be used. The barotropic equation of state is suitable for isothermal fluid flow model. It describes isentropic (reversible) processes, and implies a constant sound speed. It is given by $p = p_0 + a^2(\rho \rho_0$).
- p 0 Initial pressure value (*Pa*) in the equation of state calculations.
- rho 0 Initial value of density (kg/m^3) in the equation of state calculation.
- a2 *a* is a constant in the barotropic equation of state. The value of *a* can be taken roughly as the speed of sound. For this example problem with water as the fluids, using $a^2 = 1.e7$ has the same order of magnitude as that of the square of sound speed. This is the recommended value to use.

The Components Block:

```
[ Components ]
  [./ pipe1 ]
   type = Pipe
   eos = eos
    # geometry
   position = '000'orientation = '1 0 0'
   Dh = 0.01
   length = 1.0n_elems = 10
   A = 7.854e-5
```

```
f = 0.01[\ldots][./ inlet ]
   type = TimeDependentVolume
   input = ' pipe1 ( in )'
  p_b c = 105 e3eos = eos
  [../]
  [./ outlet ]
   type = TimeDependentVolume
   input = 'pipe1 (out)'p_bc = 1e5eos = eos
 [\ldots][]
```


The Preconditioning Block:

```
[ Preconditioning ]
 [./ SMP_PJFNK ]
   type = SMP
   full = true
  solve_type = 'PJFNK '
 [../]
[]
```


solve_type PJFNK solver will be used for this problem.

```
The Executioner Block:
```

```
[ Executioner ]
 type = Transient
 scheme = 'implicit - euler '
 dt = 1.25e-2dtmin = 1.e-5nl_{rel\_tol} = le -8nl_abs\_tol = 1e-6nl_max\_its = 15l\_tol = 1e-6l_max\_its = 30start_time = 0.0
 end_time = 250.0num_steps = 500
  [./ Quadrature ]
   type = TRAP
   order = FIRST
  [../]
[]
```


The Outputs Block:

```
[ Outputs ]
 [./ out ]
   type = Exodus
   use_displaced = true
   output_initial = true
   sequence = false
    append_displaced = true
  [\ldots][./ console ]
   type = Console
```

```
perf_log = true
  [../]
[]
```


5.2 Example 2: Use Functions to Set Initial Conditions for a Simple Pipe Flow Problem

5.2.1 Problem Description

This example illustrates how to use functions to set the initial conditions. The example used here is to set the initial pressure distribution in a pipe for an isothermal flow through one simple pipe with boundary conditions set by time dependent volumes (TDV).

Functions: Initial pressure distribution in the pipe Axis = 0 The axis used $(0, 1, \text{ or } 2 \text{ for } x, y, \text{ or } z)$ if this is to be a function of position. Note that for RELAP-7 1-D component such as a pipe, we only use x coordinate in the calculations therefore we only need to set $Axis = 0$. Type = PiecewiseLinear $x = 0$ 3' This is the pipe axial direction spatial coordinate relative to the starting point $y = '1.05e51e5'$

Initial velocity distribution in the pipe $Axis = 0$ Type = PiecewiseLinear $x = '03'$ $y = '33'$

Fig. 3 shows the plot of pressure versus pipe length for this case.

Figure 3. Pressure vs length for an isothermal pipe flow problem with initial pressure set by functions

5.2.2 Input File

The input file for this example is shown as follows:

```
#
# Isothermal flow through one simple pipe with B.C. set by TDVs and I.C. set by functions
#
[GlobalParams]
 model_type = 2
 scaling_factor_var = '1e4 1.0'
 stabilization_type = 'SUPG'
[]
[EoS]
  [./eos]
   type = BarotropicEquationOfState
   p_0 = 1.e5
```

```
rho_0 = 1.e3a2 = 1.e7[\ldots]\Box[Functions]
 # initial pressure distribution in the pipe
 [./p\_func]axis = 0type = PiecewiseLinear
   x = '0 3'
   y = '1.05e5 1e5'
 [\cdot,\cdot/]# initial velocity distribution in the pipe
 [./v_func]
   axis = 0type = PiecewiseLinear
   x = '0 3'
   y = '3 3'
 [\ldots][]
[Components]
 [./pipe1]
   type = Pipe
    eos = eos
   position = '020'orientation = '1 1 1'
   Dh = 0.01
   length = 3.0n_elems = 10
   A = 7.854e-5f = 0.01P_{\text{r}}func = p_{\text{r}}func
   V_func = v_func[\ldots][./inlet]
   type = TimeDependentVolume
    input = 'pipe1(in)'
```

```
eos = eos
   p\_bc = 1.05e5[\ldots][./outlet]
   type = TimeDependentVolume
   input = 'pipe1(out)'
   eos = eos
   p\_bc = 1.0e5[../]
[]
[Preconditioning]
 [./SMP_PJFNK]
  type = SMP
   full = true
   solve_type = 'PJFNK'
 [\ldots][[Executioner]
 type = Transient
 dt = 0.5dtmin = 1.e-5[Executioner]
 type = Transient
 dt = 0.5dtmin = 1.e-5petsc_options_iname = '-mat_fd_type -mat_mffd_type -pc_type -ksp_gmres_restart'
 petsc_options_value = ' ds ds ds lu 30'
 nl rel tol = 1e-8nl\_abs\_tol = 1e-8nl_max_its = 10
 l\_tol = 1e-4l_max\_its = 60start_time = 0.0
```

```
num_steps = 30
  [./Quadrature]
    type = TRAP
    order = FIRST
  [\,.\,.\,/][]
[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\ldots][./console]
    type = Console
    perf_log = true
  [\ldots]\lceil]
```
5.2.3 Description of the Input File

The following will provde explanations to the input parameters that did not exist in Example 1.

The Functions Block:

```
[ Functions ]
 # initial pressure distribution in the pipe
  [./ p_func]axis = 0type = PiecewiseLinear
   x = '0 3'
   y = '1.05e5 1e5'
  [\ldots]# initial velocity distribution in the pipe
 [\,.\,/\,v_ffunc]
```

```
axis = 0type = PiecewiseLinear
   x = '0 3'
   y = '3 3'
 [../]
[]
```
[./p_func] Subblock for the pressure distribution function.

x The coordinate used for the x-axis data.

y The initial pressure distribution function data point values.

The Components Block:

```
[ Components ]
  [./ pipe1 ]
    type = Pipe
    eos = eos
    position = '020'orientation = '1 1 1'
    Dh = 0.01
    length = 3.0n_elems = 10
    A = 7.854e-5f = 0.01P_{\text{r}}func = p_{\text{r}}func
    V_func = v_func[\ldots][./ inlet ]
    type = TimeDependentVolume
    input = ' pipe1 ( in )'
    eos = eos
```

```
p_bc = 1.05e5[\ldots][./outlet]
   type = TimeDependentVolume
   input = 'pipe1 (out)'eos = eos
   p_{b}c = 1.0e5[\ldots][]
```
- P_func Use the pressure function defined in the Functions block to set the initial pressure value.
- V_func Use the velocity function defined in the Functions block to set the initial velocity value.

The Executioner Block:

```
[ Executioner ]
 type = Transient
 dt = 0.5dtmin = 1.e-5[ Executioner ]
 type = Transient
 dt = 0.5dtmin = 1.e-5petsc_options_iname = '- mat_fd_type - mat_mffd_type -pc_type '
 petsc_options_value = ' ds ds ds lu'
 nl_{rel\_tol} = 1e-8nl abs tol = 1e - 8nl_max\_its = 10l\_tol = 1e-4l_max\_its = 60start_time = 0.0
 num_steps = 30
```

```
[./ Quadrature ]
    type = TRAP
    order = FIRST
  [\ldots]\lceil]
  nl_{rel\_tol} = le -8nl_abs\_tol = 1e-8nl_max\_its = 101_{\text{tol}} = 1e-4l_max_its = 60
  start_time = 0.0
  num_steps = 30
  [./ Quadrature ]
    type = TRAP
    order = FIRST
  [\ldots][]
```
petsc_options_iname Names of PETSc name and value pairs. -mat_fd_type = ds is an option to control how the Jacobian matrix is approximated by using the finite differencing method. $-mat_mffd_type = ds$ is an option to control how matrix-free operation is approximated by using the finite difference method. Users are recommended to refer to the PETSc manual for other options.

petsc options value Values of PETSc name/value paris.

5.3 Example 3: Two Phase Flow Through a Pipe - HEM Model

5.3.1 Problem Description

Two phase flow with HEM model through one simple pipe with boundary conditions set by time dependent volumes and initial conditions set by functions. The initial conditions are close to steady state solutions; therefore the simulation quickly converges to the steady state.

The following is the description of the functions defined in the Functions block: Initial pressure distribution in the pipe $Axis = 0$ Type = PiecewiseLinear $x = '01'$ $y = '7.01e67e6'$

Initial velocity distribution in the pipe $Axis = 0$ Type = PiecewiseLinear $x = '01'$ $y = '1.35 2.1'$

Initial temperature distribution in the pipe $Axis = 0$ Type = PiecewiseLinear $x = '00.041'$ y = '517 517.343 517.253'

Initial void fraction distribution in the pipe $axis = 0$ type = PiecewiseLinear $x = '00.041'$ $y = '00.037'$

The parameters and functions used for the pipe component are the following: Position = $'000'$ Orientation = 100

Area = 7.854*e*−5*m* 2 Diameter = 0.01 m Length = $1. m$ Number of elements = 100 Friction coefficient $= 0.1$ Convective heat transfer coefficient = 1e4 Heat flux perimeter $= 0.031416$ Wall temperature = 528 K The name of EOS to use $=$ two $_{\text{phase}.\text{eos}}$ Initial condition determined by functions which are close to SS solutions Function which defines pressure as a function of $x = p$ func Function which defines velocity as a function of $x = v$ func Function which defines temperature as a function of $x = temp_func$ Function which defines vapor volume fraction as a function of $x = void$ func

The inlet boundary conditions: Vapor volume fraction $= 0$. The name of EOS to use $=$ two $_{\text{phase}.\text{eos}}$

The outlet boundary conditions: Vapor volume fraction $= 0.5$ The name of EOS to use $=$ two $_{\text{phase}.\text{eos}}$

5.3.2 Input File

```
#
# Two phase flow with HEM model through one simple pipe with B.C. set by TDVs and
# I.C. set by functions. The I.C.s are close to steady state solutions; therefore
# the simulation quickly converges to the steady state.
#
[GlobalParams]
 model_type = 32
 stabilization_type = 'NONE'
 scaling_factor\_var = '1e+4 1 1e-2'
 gravity = '0.0, 0.0, -9.8'\Box[EoS]
 [./two_phase_eos]
  type = TwoPhaseStiffenedGasEOS
 [\ldots][]
[Functions]
 # initial pressure distribution in the pipe
 [./p_func]
   axis = 0type = PiecewiseLinear
   x = '0 1'
   y = '7.01e6 7e6'
 [\,\ldots\,]# initial velocity distribution in the pipe
 [\cdot/\text{v\_func}]axis = 0type = PiecewiseLinear
   x = '0 1'
   y = '1.35 \t2.1'[\ldots]
```
initial temperature distribution in the pipe

```
[./temp_func]
   axis = 0type = PiecewiseLinear
   x = '0 0.04 1'y = '517 517.343 517.253'[\ldots]# initial void fraction distribution in the pipe
 [./void_func]
   axis = 0type = PiecewiseLinear
   x = '0 \t 0.04 \t 1'y = '0 \t 0. \t 0.37'[\ldots]\Box[Components]
 [./pipe1]
   type = Pipe
   position = '0 0 0'orientation = '1 0 0'
   A = 7.854e-5Dh = 0.01length = 1.
   n_elems = 100
   f = 0.1Hw = 1e4Phf = 0.031416000000
   Tw = 528eos = two_phase_eos
   # initial condition determined by functions which are close to steady state solutions
   P_{\text{r}}func = p_{\text{r}}func
   V_func = v_funcT_func = temp_func
   volume_fraction_vapor_func = void_func
 [\ldots][./inlet]
   type = TimeDependentVolume
   input = 'pipe1(in)'
```

```
p_bc = 7.01e6
   T_{DC} = 517.volume_fraction_vapor_bc = 0.
   eos = two_phase_eos
  [\ldots][./outlet]
   type = TimeDependentVolume
   input = 'pipe1(out)'
   p_bc = 7.0e6T_bc = 517volume_fraction_vapor_bc = 0.5
   eos = two_phase_eos
 [\ldots][]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
    solve_type = 'PJFNK'
   petsc_options_iname = '-mat_fd_type -mat_mffd_type -pc-type'
   petsc_options_value = 'ds ds lu'
 [\,.\,.\,/][]
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1e-1dtmin = 1.e-3nl rel tol = 1e-9nl\_abs\_tol = 1e-9nl_max\_its = 50l\_tol = 1e-3l_max\_its = 60start_time = 0.0
```

```
num_steps = 50
  [./Quadrature]
    type = TRAP
    order = FIRST
  [\ldots]\Box[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\ldots][./console]
    type = Console
    perf_log = true
  [\ldots]\lceil]
```
5.3.3 Description of the Input File

The following are the detailed explanations of the input parameters that did not exit in the previous examples.

The Global Parameters Block:

```
[ GlobalParams ]
 model_type = 32
 stabilization_type = 'NONE '
 scaling_factor\_var = '1e+4 1 1e-2'
  qravity = '0.0, 0.0, -9.8'[]
```
model_type model_type=32 indicates that the HEM two-phase flow model will be used for this problem.

gravity The gravity acceleration vector.

The Equation of State Block:

```
[ EoS ]
  [./ two_phase_eos ]
    type = TwoPhaseStiffenedGasEOS
  [\ldots][]
```
type Two phase stiffened gas equation of state will be used for this problem.

The Components Block:

```
[ Components ]
  [./ pipe1 ]
   type = Pipe
    position = '000'orientation = '1 0 0'
    A = 7.854e-5Dh = 0.01
    length = 1.
    n_elems = 100
    f = 0.1Hw = 1e4Phf = 0.031416000000
    Tw = 528eos = two_phase_eos
    P_{\text{tunc}} = p_{\text{tunc}}V_func = v_func
    T_func = temp_func
    volume_fraction_vapor_func = void_func
  [\ldots][./ inlet ]
    type = TimeDependentVolume
    input = 'pipe1 (in)'p_{b}c = 7.01e6T_{bc} = 517.volume_fraction_vapor_bc = 0.
```

```
eos = two_phase_eos
  [\ldots][./ outlet ]
   type = TimeDependentVolume
   input = ' pipe1 ( out )'
   p_bc = 7.0e6T_bc = 517volume_fraction_vapor_bc = 0.5
   eos = two_phase_eos
 [../]
[]
```


5.4 Example 4: Two Phase Flow Through a Pipe - 7-Equation Model

5.4.1 Problem Description

This example shows a two phase flow with the 7-equation model through one simple pipe with boundary conditions set by Inlet and Outlet components at the pipe inlet and outlet ends respectively. The initial conditions are set by functions. The initial conditions are set to be close to steady state solutions; therefore the simulation quickly converges to steady state solutions.

5.4.2 Input File

The input file for this pipe flow case with the 7-equation two-phase flow model is shown below:

```
[GlobalParams]
 model_type = 7
 qlobal_init_T = 517.252
 global_init_P = 7.0e6
 global_init_V = 0
 global_init_volume_fraction_vapor = 0.95
 scaling_factor_var_2phase = '1
                              1e1 1e1 1e-3
                              1e1 1e1 1e-3'
 phase_interaction = true
 pressure_relaxation = true
 velocity_relaxation = true
 interface_transfer = true
 wall_mass_transfer = true
 stabilization_type = LAPIDUS
 specific_interfacial_area_max_value = 1700
[]
[Functions]
  # initial pressure distribution in the pipe
 [./p_func]
   axis = 0type = PiecewiseLinear
   x = '0 3.66'
```

```
y = '7.005e6 7e6'
 [\ldots]# initial velocity distribution in the pipe
 [\cdot/\text{v\_func}]axis = 0type = PiecewiseLinear
   x = '0 3.66'
   y = '6 6.6'
 [\ldots]# initial temperature distribution in the pipe
  [./temp_func]
   axis = 0type = PiecewiseLinear
   x = '0 3.66'
   y = '517.252 517.817'
 [\ldots]# initial void fraction distribution in the pipe
 [./void_func]
   axis = 0type = PiecewiseLinear
   x = '0 3.66'
   y = '0.95 0.956'[\ldots]\lceil]
[EoS]
  [./eos_liquid]
   type = StiffenedGasEquationOfStateLiquid
   gamma = 2.35q = -1167e3q_prime = 0
   p\_inf = 1.e9cv = 1816[\ldots][./eos_vapor]
   type = StiffenedGasEquationOfStateVapor
```

```
gamma = 1.43
    q = 2030e3
    q prime = -23e3p_{in}f = 0cv = 1040[\cdot,\cdot/][]
[Components]
  [./pipe]
   type = Pipe
    eos_liquid = eos_liquid
    eos_vapor = eos_vapor
   position = '0 0 0'orientation = '0 0 1'
   A = 1.907720E - 04Dh = 1.698566E-02length = 3.66f = 1.698566E-02Hw_lliquid = 1000.0
   Hw_vapor = 1000.0Phf = 0.0489623
    Tw = 550n_elems = 50
   P_liquid_func = p_func
    P_vapor_func = p_func
   V_liquid_func = v_func
   V_vapor_func = v_func
    T_liquid_func = temp_func
    T_vapor_func = temp_func
    volume_fraction_vapor_func = void_func
  [\ldots][./inlet]
   type = Inlet
    input = 'pipe(in)'
   p_liquid = 7.005e6p_vapor = 7.005e6
    T_liquid = 517.252
```
 $T_{vapor} = 517.252$

```
volume_fraction_vapor = 0.95
   eos_liquid = eos_liquid
   eos_vapor = eos_vapor
  [\ldots][./outlet]
   type = Outlet
   input = 'pipe(out)'
   p\_vapor = 7.0e6p_liquid = 7.0e6
   eos_liquid = eos_liquid
   eos_vapor = eos_vapor
 [\ldots][[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
   solve_type = 'PJFNK'
 [\ldots]\Box[Executioner]
 type = Transient
 dt = 1e-1dtmin = 1.e-5nl rel tol = 1e-10nl\_abs\_tol = 1e-8nl_max_its = 30
 l\_tol = 1e-3l_max\_its = 30petsc_options_iname = '-mat_mffd_type -ksp_gmres_restart'
 petsc_options_value = 'ds 300'
 start_time = 0.0
 num_steps = 100
 [./Quadrature]
   type = TRAP
```

```
order = FIRST
  [\ldots][]
[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\,.\,.\,]/[./console]
    type = Console
    perf_log = true
  [\ldots][]
```
5.4.3 Description of the Input File

The following provides the explanations of the input parameters that did not exist in the previous examples:

The Global Parameters Block:

```
[ GlobalParams ]
 model_type = 7global\_init_T = 517.252global_init_P = 7.0 e6
 global_init_V = 0
 global_init_volume_fraction_vapor = 0.95
  scaling_factor_var_2phase = '1
                               1e1 1e1 1e-3
                               1e1 1e1 1e-3'
 phase_interaction = true
 pressure_relaxation = true
 velocity_relaxation = true
  interface_transfer = true
```

```
wall_mass_transfer = true
 stabilization_type = LAPIDUS
 specific_interfacial_area_max_value = 1700
[]
```


The Equation of State Block:

```
[ EoS ]
 [./ eos_liquid ]
   type = StiffenedGasEquationOfStateLiquid
   qamma = 2.35q = -1167e3q prime = 0p\_inf = 1.e9cv = 1816[\ldots][./ eos_vapor ]
   type = StiffenedGasEquationOfStateVapor
    gamma = 1.43
```

```
q = 2030e3q prime = -23e3p\_inf = 0cv = 1040[../]
[]
```


The Components Block

```
[ Components ]
 [./ pipe ]
   type = Pipe
   eos_liquid = eos_liquid
   eos_vapor = eos_vapor
   position = '0 0 0'orientation = '1 0 0'
   A = 1.907720E - 04Dh = 1.698566E - 02length = 3.66f = 1.698566E - 02Hw_lliquid = 1000.0
   Hw_vapor = 1000.0Phf = 0.0489623
   Tw = 550n_elems = 50
```

```
P_liquid_func = p_func
    P_vapor_func = p_func
   V_liquid_func = v_func
   V_vapor_func = v_func
   T_liquid_func = temp_func
   T_vapor_func = temp_func
   volume_fraction_vapor_func = void_func
  [\ldots][./ inlet ]
   type = Inlet
   input = 'pipe (in)'p<sup>1iquid = 7.005e6</sup>
   p_vapor = 7.005e6T_{\text{light}} = 517.252T_vapor = 517.252volume_fraction_vapor = 0.95
   eos_liquid = eos_liquid
   eos_vapor = eos_vapor
  [\ldots][./ outlet ]
   type = Outlet
   input = ' pipe ( out )'
   p_vapor = 7.0e6p<sup>1iquid = 7.0 e6</sup>
   eos_liquid = eos_liquid
   eos_vapor = eos_vapor
  [\ldots][]
```


5.5 Example 5: A Core Channel Problem

Fuel Gap Clad **Coolant Flow Coolant Flow**

5.5.1 Problem Description

Figure 4. Diagram of a core channel problem

This example simulates single phase fluids flow and heat transfer in a core channel, as schematically shown in Fig. 4. This problem similates fluids flow in one subchannel with a single fuel rod as the heat source. The boundary conditions are applied to the ends of the core channel. The reactor power = 77337.69407 *W* is used for the core channel. Other parameters used are the following:

Fluids Flow: Cross section flow area = $8.7878e-5$ m^2 Hydraulic Diameter = 0.01179 m Length $= 4 \text{ m}$ Friction coefficient = 0.01 Convective heat transfer coefficient = 5.33e4 W/m^2 $*$ K Heat flux perimeter $= 0.029832559676$ m Number of elements = 20

Heat Structure: Dimension of mesh used for heat conduction $= 1$ Geometry type of fuel = cylinder Heat structure names = 'fuel gap clad' Number of heat structures $= 3$ Width of each heat structure = '0.004096 0.0001 0.000552' m Number of elements of each heat structure = '10 1 2' Name of materials used in the heat structure = 'fuel-mat gap-mat clad-mat' Fraction of reactor power goes into heat structure = '1.0 0.0 0.0' Initial Solid Temperature = 559.15 K

The boundary conditions are the following:

Inlet: Pressure = 155.483e5 Pa Temperature = 559.15 K

Outlet: Pressure $= 155.$ e $5Pa$ Temperature = 559.15 K

The solid material properties $(k = Thermal conductivity, Cp = heat capacity, rho = Density)$ are:

Fuel: $k = 2.5$ $Cp = 300$ $rho = 1.032e4$ Gap: $k = 0.6$ $Cp = 1$. $rho = 1$. Clad: $k = 21.5$ $Cp = 350.$

 $rho = 6.55e3$

5.5.2 Input File

The follwoing shows the input file for the Core Channel example. Please note that the mesh used for this problem does not correspond to what is shown in Fig. 4.

```
[GlobalParams]
 global_init_P = 155.e5
 global_init_V = 0.
 global\_init_T = 559.15model_type = 3
 stabilization_type = 'SUPG'
 scaling_factor_var = '1e4 1e1 1e-2'
 temperature_sf = '1e-2'
[]
[EoS]
 [./eos]
    type = NonIsothermalEquationOfState
   p_0 = 155.e5rho_0 = 686.0a2 = 1.e7beta = .46e-3cv = 5.5e3e_0 = 3075325
    T_0 = 559.15[\ldots][]
[Materials]
  [./fuel-mat]
   type = SolidMaterialProperties
   k = 2.5Cp = 300.
    rho = 1.032e4[\ldots][./gap-mat]
```

```
type = SolidMaterialProperties
   k = 0.6Cp = 1.
   rho = 1.
  [\ldots][./clad-mat]
   type = SolidMaterialProperties
   k = 21.5Cp = 350.
   rho = 6.55e3[\ldots][]
[Components]
  [./reactor]
   type = Reactor
   initial_power = 77337.69407
  [\ldots][./CCH1]
    type = CoreChannel
    eos = eos
   position = '0 0 0'orientation = '0 0 1'
   A = 8.7878e-5Dh = 0.01179length = 4n elems = 20
   f = 0.01Hw = 5.33e4Phf = 0.029832559676
   Ts_init = 559.15
   dim_hs = 1fuel_type = cylinder
    name_of_hs = 'fuel gap clad'
    n_heatstruct = 3
   width_of_hs = '0.004096 0.0001 0.000552'
   elem_number_of_hs = '10 1 2'
   material_hs = 'fuel-mat gap-mat clad-mat'
   power_fraction = '1.0 0.0 0.0'
  [\ldots]
```
```
[./inlet]
    type = TimeDependentVolume
    input = 'CCH1(in)'p_bc = 155.483e5
   T bc = 559.15eos = eos
  [\ldots][./outlet]
   type = TimeDependentVolume
    input = 'CCH1(out)'
   p_{bc} = '155. e5'T_bc = 559.15
   eos = eos
 [../]
[]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
   solve_type = 'PJFNK'
 [\ldots][]
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1.e-2 #1.e-5
 dtmin = 1.e-5nl_rel_tol = 1e-9
 nl abs tol = 1e-8nl_max_its = 20
 l\_tol = 1e-3l_max\_its = 30start_time = 0.0
 num_steps = 50
```

```
[./Quadrature]
     type = TRAP
     order = FIRST
  [\ldots]\lceil]
[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\ldots][./console]
    type = Console
    perf_log = true
  [\ldots][]
```
5.5.3 Description of the Input File

The Global Parameter Block:

```
[ GlobalParams ]
 global_init_P = 155. e5
 global_init_V = 0.
 global\_init_T = 559.15model_type = 3
 stabilization_type = 'SUPG '
 scaling_factor\_var = '1e4 1e1 1e-2'temperature_sf = '1e-2'[]
```
temperature sf Scaling factor for the temperature variable in solid materials.

The Materials Block:

```
[ Materials ]
  [./ fuel - mat ]
   type = SolidMaterialProperties
   k = 2.5Cp = 300.rho = 1.032 e4
  [\ldots][./ gap - mat ]
   type = SolidMaterialProperties
   k = 0.6Cp = 1.
   rho = 1.
 [\ldots][./clad-mat]
   type = SolidMaterialProperties
   k = 21.5Cp = 350.rho = 6.55e3[../]
[]
```
- k Thermal conductivity.
- Cp Specific heat.
- rho Density of solid materials.

```
[ Components ]
 [./ reactor ]
   type = Reactor
    initial_power = 77337.69407
 [\ldots][./ CCH1 ]
   type = CoreChannel
   eos = eos
   position = '0 0 0'orientation = '0 0 1'
   A = 8.7878e-5
```

```
Dh = 0.01179
   length = 4n_elems = 20
   f = 0.01Hw = 5.33e4Phf = 0.029832559676
   Ts_init = 559.15
   dim_h s = 1fuel_type = cylinder
   name_of_hs = ' fuel gap clad '
   n_heatstruct = 3
   width_of_hs = '0.004096 0.0001 0.000552 '
   elem_number_of_hs = '10 1 2'
   material_hs = 'fuel-mat gap-mat clad-mat'
   power_fraction = '1.0 0.0 0.0 '
 [\ldots][./ inlet ]
   type = TimeDependentVolume
   input = 'CCH1 (in)'p_bc = 155.483e5T_{\text{loc}} = 559.15eos = eos
 [\ldots][./ outlet ]
   type = TimeDependentVolume
   input = 'CCH1(out)'p_{b}c = '155.e5'T_{bc} = 559.15eos = eos
 [\ldots][]
```


5.6 Example 6: A Two Pipes Flow Problem

5.6.1 Problem Description

Figure 5. Diagram of a two pipes flow problem

This example demonstrates flow through two pipes with different parameters connected by a branch. There is no heat exchange through the pipe walls for this case. The following are the input parameters for each component:

Pipe 1: Hydraulic Diameter = .01 m Area = $1.0e-4$ m^2 Length $= 1$ m Friction coefficient = .01 Convective heat transfer coefficient $= 0$

Pipe 2: Hydraulic Diameter = .02 m Area = $4e-4$ m^2 Length $= 1.5$ m Friction = .02 Convective Heat Transfer Coefficient $= 0$

Branch: Form loss coefficients = '5 5' Area = $1.5e-4$ m^2

Initial pressure = 1e5 Pa

Inlet: Pressure $= 1.01e5$ Pa Temperature = $300 K$

Outlet: Pressure = 1e5 Pa

The following figure shows the results of the pressure versus pipes length for this case.

Figure 6. Pressure vs. length for the two pipes flow problem

The results of the pressure difference can be checked by doing hand calculations by summing ∆*P* using:

$$
\Delta P = \frac{fL\rho u^2}{2D_h} \tag{2}
$$

and:

$$
\Delta P = \frac{k \rho u^2}{2} \tag{3}
$$

5.6.2 Input File

The input file for this example problem is listed as follows:

```
[GlobalParams]
 model_type = 3
 gravity = '0 0 0'stabilization_type = 'SUPG'
 scaling_factor_var = '1.e3 1.e-1 1.e-3'
 global_init_T = 300
 global_init_P = 1.0e5
 global_init_V = 1
[]
[EoS]
   [./eos]
    type = NonIsothermalEquationOfState
    p_0 = 1.e5rho_0 = 1.e3a2 = 1.e7beta = .46e-3cv = 4.18e3e_0 = 1.254e6T_0 = 300[\ldots][]
[Components]
  [./pipe1]
   type = Pipe
   eos = eos
   position = '0 0 0'orientation = '1 0 0'
   length = 1n_elems = 25
   A = 1.0e-4Dh = 0.01
   f = .01Hw = 0.[\ldots]
```

```
[./Branch1]
   type = Branch
   inputs = 'pipe1(out)'
   outputs = 'pipe2(in) '
   K = '5 \ 5'Area = 1.5e-4Initial_pressure = 1e5
   eos = eos
 [\ldots][./pipe2]
   type = Pipe
   eos = eos
   position = '1.001 0 0'
   orientation = '1 0 0'
   length = 1.5n_elems = 25
   A = 4e-4Dh = 0.02f = .02Hw = 0.[../]
 [./inlet]
   type = TimeDependentVolume
   input = 'pipe1(in)'
   p_bc = 1.01e5T_bc = 300eos = eos
 [../]
 [./outlet]
   type = TimeDependentVolume
   input = 'pipe2(out)'
   p\_bc = 1e5eos = eos
 [../]
[]
```

```
[Preconditioning]
```

```
[./SMP_PJFNK]
  type = SMP
  full = true
  solve_type = 'PJFNK'
[\ldots]\Box[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1e-2
 dtmin = 1e-5
 nl_rel_tol = 1e-8
 nl\_abs\_tol = 1e-6nl_max_its = 30
 l tol = 1e-4
 l_max\_its = 30petsc_options_iname = '-mat_fd_coloring_err -mat_fd_type -mat_mffd_type -pc_type'
 petsc_options_value = '1.e-10 ds ds lu'
 start_time = 0.0
 end_time = 10.0num_steps = 5000
 [./Quadrature]
   type = TRAP
   order = FIRST
 [\ldots][]
[Outputs]
 [./out]
   type = Exodus
   use_displaced = true
   output_initial = true
   sequence = false
   append_displaced = true
```

```
[\ldots][./console]
   type = Console
   perf_log = true
 [../]
[]
```
5.6.3 Description of the Input File

The only input parameters that need explanations are those in the Branch subblock.

```
[./ Branch1 ]
 type = Branch
 inputs = ' pipe1 ( out )'
 outputs = 'pipe2(in)'
 K = '5 5'Area = 1.5e-4Initial_pressure = 1 e5
 eos = eos
[../]
```


5.7 Example 7: A Volume Branch Case - Three Pipes In and Two Pipes Out

5.7.1 Problem Description

Figure 7. Diagram of a volume branch case with three pipes flowing in and two pipes flowing out

This example shows a volume branch case which connects three pipes with water flowing into them and two pipes with water flowing out of them. The pipe sizes are all the same, but the boundary conditions vary. The volume branch model includes the volume effects of a junction. The input parameters used in this example are listed in the following:

Pipes: Area = $3.14e-4$ m^2 Diameter = 0.02 m Length $= 1$ m Number of elements in pipe = 10 Friction coefficient = 0.01

Branch1: Type = VolumeBranch $inputs = 'pipe1(out) pipe2(out) pipe3(out)'$ $outputs = 'pipe4(in) pipe5(in)'$ Form loss coefficients = '0.01 0.01 0.01 0.01 100' Area = 3.14*e*−2*m* 2 volume = 3.14*e*−2*m* 3 Initial Temperature = 628.15 K

Inlet 1: type = TimeDependentJunction Velocity $= 1.0$ m/s Temperature = 628.15 K

Inlet 2: type = TimeDependentJunction Velocity = 1.0 m/s Temperature = 628.15 K

Inlet 3: type = TimeDependentJunction Velocity = 10.0 m/s Temperature = 528.15 K

Outlet 1: type = TimeDependentVolume Pressure = 1.0e5 Pa Temperature = 628.15 K

Outlet 2: type = TimeDependentVolume Pressure $= 1.5e5$ Pa Temperature = 628.15 K

5.7.2 Input File

```
[GlobalParams]
 global_init_P = 1.5e5
 global_init_V = 1
 global\_init_T = 628.15model_type = 3
 stabilization_type = 'SUPG'
 scaling_factor_var = '1e4 1 1e-3'
[]
[EoS]
 active = 'eos'
 [./eos]
   type = NonIsothermalEquationOfState
   p_0 = 1e5rho_0 = 865.51a2 = 5.7837e6beta = 2.7524e-4cv = 1272.0e_0 = 7.9898e5
   T_0 = 628.15[\,.\,.][]
[Components]
  [./pipe1]
   type = Pipe
   eos = eos
   position = '0 0 0'orientation = '0 0 1'
   A = 3.14e-4Dh = 0.02
   length = 1n_elems = 10
   f = 0.01Hw = 0[\ldots]
```

```
[./pipe2]
  type = Pipe
 eos = eos
 position = '-1.5 0 1.25'
 orientation = '1 0 0'
 A = 3.14e-4Dh = 0.02length = 1
 n_elems = 10
 f = 0.01Hw = 0[\ldots][./pipe3]
 type = Pipe
 eos = eos
 position = ' -1.5 0 1.75'orientation = '1 0 0'
 A = 3.14e-4Dh = 0.02length = 1
 n_elems = 10
 f = 0.01Hw = 0[\ldots][./pipe4]
 type = Pipe
 eos = eos
 position = '0 0 2'orientation = '0 0 1'
 A = 3.14e-4Dh = 0.02length = 1
 n_elems = 10
  f = 0.01Hw = 0[../]
[./pipe5]
```

```
type = Pipe
  eos = eos
  # geometry
 position = '0.5 0 1.5'
 orientation = '1 0 0'
 A = 3.14e-4Dh = 0.02length = 1n_elems = 10
 f = 0.01Hw = 0[\ldots][./branch1]
 type = VolumeBranch
 eos = eos
 center = '0 0 1.5'
 inputs = 'pipe1(out) pipe2(out) pipe3(out)'
 outputs = 'pipe4(in) pipe5(in)'
 K = '0.01 0.01 0.01 0.01 100'Area = 3.14e-2volume = 3.14e-2initial_T = 628.15[\ldots][./inlet1]
 type = TimeDependentJunction
 input = 'pipe1(in)'
 eos = eos
 v_bc = 1.0T_bc = 628.15[\ldots][./inlet2]
 type = TimeDependentJunction
 input = 'pipe2(in)'eos = eos
 v_{bc} = 1.0T_{DC} = 628.15[\ldots]
```

```
[./inlet3]
   type = TimeDependentJunction
   input = 'pipe3(in)'
   eos = eos
   v_bc = 10.0T bc = 528.15[\ldots][./outlet1]
   type = TimeDependentVolume
   input = 'pipe4(out)'
   eos = eos
   p_bc = '1.0e5'T_bc = 628.15
 [../]
 [./outlet2]
   type = TimeDependentVolume
   input = 'pipe5(out)'eos = eos
   p\_bc = '1.5e5'T_bc = 628.15[\ldots][]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
    solve_type = 'PJFNK'
 [../]
\lceil]
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
```
 $dt = 0.2$

```
dtmin = 1e-10
 # setting time step range
 [./TimeStepper]
   type = FunctionDT
   time_t = '0 0.05 0.051 0.3 0.31 2 2.1 1e5'
   time_dt ='1.e-2 1.e-2 5e-2 5e-2 2e-1 0.2 0.5 0.5 '
  [\ldots]nl_rel_tol = 1e-6
 nl\_abs\_tol = 1e-7nl_max\_its = 30l\_tol = 1e-6l_max\_its = 100petsc_options_iname = '-pc_type -ksp_gmres_restart'
 petsc_options_value = 'lu 300'
 start_time = 0.0
 num_steps = 500
 [./Quadrature]
   type = TRAP
   order = FIRST
 [\ldots][]
[Outputs]
 [./out]
   type = Exodus
   use_displaced = true
   output_initial = true
   sequence = false
   append_displaced = true
 [\ldots][./console]
   type = Console
   perf_log = true
 [\ldots]
```
5.7.3 Description of the Input File

```
[./ branch1 ]
  type = VolumeBranch
  eos = eos
  center = '0 \t0 \t1.5'inputs = 'pipe1 (out) pipe2 (out) pipe3 (out)'outputs = 'pipe4(in) pipe5(in)'
  K = '0.01 0.01 0.01 0.01 0.01 100'Area = 3.14e-2volume = 3.14e-2initial_T = 628.15[\ldots]
```
center The (x, y, z) coordinate of the center of the volume branch.

volume The volume of VolumeBranch component.

```
[./ TimeStepper ]
 type = FunctionDT
 time_t = '0 0.05 0.051 0.3 0.31 2 2.1 1e5'
 time_dt ='1.e-2 1.e-2 5e-2 5e-2 2e-1 0.2 0.5 0.5'
[\ldots]
```
[./TimeStepper] Subblock to define time step size as a function of simulation time.

type **FunctionDT** type to be used.

time t The value of time t.

time_dt The value of time step.

5.8 Example 8: A Simple Pipe Loop with Pump

5.8.1 Problem Description

Figure 8. Diagram of a simple loop of pipes connected by branches and a pump

This example shows a loop made up of 5 pipes, 3 branches and a pump. The pump acts as a junction, connecting pipes 1 and 2, and pipe 5 is used as an outlet to help control the pressure. The input parameters used for the Pump model are the following:

Pump head $= 1.0$ Form loss coefficient (in the reverse direction) = '10. 10.' Area = 0.785398163*e*−3*m* 2 Initial pressure = 1.e5 Pa

5.8.2 Input File

```
[GlobalParams]
  model_type = 3
 stabilization_type = 'SUPG'
  scaling_factor_var = '1e4 1e1 1e-2'
[]
[EoS]
  [./eos]
   type = NonIsothermalEquationOfState
   p_0 = 1.e5rho_0 = 1.e3a2 = 1.e7beta = -.46e-3cv = 4.18e3e_0 = 1.254e6T_0 = 300[\ldots][]
[Components]
  [./pipe1]
   type = Pipe
   eos = eos
   position = '0 0 0'orientation = '1 0 0'
   A = 0.785398163e-4Dh = 0.01length = 1
   n_elems = 10
   f = 0.01Hw = 0.0[\ldots][./pipe2]
   type = Pipe
   eos = eos
   position = '1 0 0'
```

```
orientation = '0 1 0'
 A = 0.785398163e-4Dh = 0.01
 length = 1n_elems = 10
 f = 0.01Hw = 0.0[\ldots][./pipe3]
 type = Pipe
 eos = eos
 position = '1 1 0'orientation = '-1 0 0'
 A = 0.785398163e-4Dh = 0.01
 length = 1
 n_elems = 10
 f = 0.01Hw = 0.0[\ldots][./pipe4]
 type = Pipe
 eos = eos
  # geometry
 position = '0 1 0'orientation = '0 -1 0'A = 0.785398163e-4Dh = 0.01length = 1
 n_elems = 10
 f = 0.01Hw = 0.0[\ldots][./pipe5]
 type = Pipe
 eos = eos
 position = '1 1 0'orientation = '0 1 0'
```

```
A = 0.785398163e-4Dh = 0.01
 length = .25n elems = 10
  f = 0.01Hw = 0.0[\ldots][./pump]
 type = Pump
 eos = eos
  inputs = 'pipe1(out)'
  outputs = 'pipe2(in)'Head = 1.0K_reverse = '10. 10.'Area = 0.785398163e-3Initial_pressure = 1.e5
[\ldots][./branch2]
 type = Branch
 eos = eos
 inputs = 'pipe2(out)'
 outputs = 'pipe3(in) pipe5(in)'
 K = '3. 3. 3.'Area = 0.785398163e-3Initial_pressure = 1.e5
[\ldots][./branch3]
 type = Branch
 eos = eos
 inputs = 'pipe3(out)'
 outputs = 'pipe4(in)'
 K = '3. 3.'Area = 0.785398163e-3Initial_pressure = 1.e5
[\ldots][./branch4]
```

```
type = Branch
```

```
eos = eos
    inputs = 'pipe4(out)'
    outputs = 'pipe1(in)'
   K = '3. 3.'Area = 0.785398163e-3Initial_pressure = 1.e5
  [\,\ldots/\,][./TDV]
   type = TimeDependentVolume
   input = 'pipe5(out)'p_bc = '1.e5'T bc = 300.0eos = eos
 [\ldots][]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
   solve_type = 'PJFNK'
 [\ldots][]
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1.e-4dtmin = 1e-7
 nl_rel_tol = 1e-6
 nl\_abs\_tol = 1e-8nl_max_its = 10
 l\_tol = 1e-8l_max\_its = 60petsc_options_iname = '-ksp_gmres_restart'
 petsc_options_value = '30'
```

```
start_time = 0.0
  num_steps = 50
  [./Quadrature]
    type = TRAP
    order = FIRST
  [\ldots][]
[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\ldots][./console]
   type = Console
    perf_log = true
  [\ldots][]
```
5.8.3 Description of the Input File

```
[./ pump ]
 type = Pump
 eos = eos
 inputs = 'pipe1 (out)'outputs = 'pipe2(in)'
 Head = 1.0K_reverse = '10. 10. '
 Area = 0.785398163e-3Initial_pressure = 1. e5
[\ldots]
```
[./pump] Subblock for the pump component.

5.9 Example 9: A Heat Exchanger Problem

5.9.1 Problem Description

Figure 9. Diagram of a heat exchanger problem

This examples illustrates how to run a case with the heat exchanger component. The heat exchanger has two inlets and two outlets, primary and secondary respectively. The primary side inlet lets in hot water, while the secondary side inlet lets in liquid at a cooler temperature. This helps cool the primary side liquid, so the primary side outlet temperature is somewhat lower while the secondary side outlet temperature is somewhat higher. This example problem is for subcooled water only. The input parameters used for this case are listed in the following:

Materials: Thermal Conductivity $= 100.0$ Density = 100.0 Specific Heat $= 100.0$

Heat Exchanger:

Area of primary pipe = 0.785398163*e*−4*m* 2 Area of secondary pipe = 0.785398163*e*−4*m* 2 Diameter of primary pipe $= 0.01$ m Diameter of secondary pipe $= 0.01$ m Length $= 1$ m Primary convective heat transfer coefficient = 1.e4 Secondary convective heat transfer coefficient = 1.e4 Primary heat flux perimeter= 0.031415926520 Secondary heat flux perimeter $= 0.031415926520$ Friction coefficient = 0.01 Initial wall temperature $= 300.0 \text{ K}$ Dimension of mesh used for wall $= 1$ Thickness of the wall between primary and secondary loop $= 0.001$ m

Primary inlet TDV: Pressure $= 1.05e5$ Pa Temperature $= 400.0 \text{ K}$

Primary outlet TDV: Pressure $= 1.e5$ Pa Temperature = 300.0 K

Secondary inlet TDV: Pressure $= 1.05e5$ Pa Temperature = 300.0 K

Secondary outlet TDV: Pressure $= 1.e5$ Pa Temperature = 300.0 K

5.9.2 Input File

```
[GlobalParams]
 global_init_P = 1.e5
```

```
global_init_V = 0.
 global_init_T = 300.
 model_type = 3
 stabilization_type = 'SUPG'
 scaling_factor_var = '1e4 1e1 1e-2'
 temperature_sf = '1e-2'
\lbrack[EoS]
  [./eos]
   type = NonIsothermalEquationOfState
   p_0 = 1.e5rho_0 = 1.e3a2 = 1.e7beta = .46e-3cv = 4.18e3e_0 = 1.254e6T_0 = 300[../]
\Box[Materials]
 [./wall-mat]
   type = SolidMaterialProperties
   k = 100.0rho = 100.0Cp = 100.0[\ldots][]
[Components]
 [./HX]
   type = HeatExchanger
   eos = eos
   eos_secondary = eos
   position = '0 0 0'orientation = '1 0 0'
   A = 0.785398163e-4A_secondary = 0.785398163e-4
   Dh = 0.01
```

```
Dh_secondary = 0.01
 length = 1n_elems = 10
 Hw = 1.e4Hw\_secondary = 1.e4Phf = 0.031415926520
 Phf_secondary = 0.031415926520
 f = 0.01f_secondary = 0.01Twall\_init = 300.0dim_wall = 1wall_thickness = 0.001
 material_wall = wall-mat
 n_wall_elems = 2
[\,\ldots\,][./primary_inlet_TDV]
 type = TimeDependentVolume
 input = 'HX(primary_in)'
 p\_bc = 1.05e5T bc = 400.0eos = eos
[\ldots][./primary_outlet_TDV]
 type = TimeDependentVolume
 input = 'HX(primary_out)'
 p_{bc} = '1.e5'T_bc = 300.0eos = eos
[\ldots][./secondary_inlet_TDV]
 type = TimeDependentVolume
 input = 'HX(secondary_in)'
 p\_bc = 1.05e5T_{\perp}bc = 300.0eos = eos
[\ldots][./secondary_outlet_TDV]
```

```
type = TimeDependentVolume
    input = 'HX(secondary_out)'
   p_bc = '1.e5'T bc = 300.0eos = eos
 [\ldots]\Box[Preconditioning]
  [./SMP_PJFNK]
   type = SMP
    full = true
   solve_type = 'PJFNK'
   line_search = basic
 [../]
[]
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1.e-3dtmin = 1e-7
 nl_rel_tol = 1e-6
 nl\_abs\_tol = 1e-8nl_max\_its = 20l tol = 1e-6
 l_max\_its = 300petsc_options_iname = '-ksp_gmres_restart -pc_type'
 petsc_options_value = '300 lu'
 start time = 0.0num_steps = 1000
 [./Quadrature]
   type = TRAP
   order = FIRST
 [\ldots][]
```

```
[Outputs]
  [./out]
    type = Exodus
    use_displaced = true
    output_initial = true
    sequence = false
    append_displaced = true
  [\ldots][./console]
    type = Console
    perf_log = true
  [\ldots][]
```
5.9.3 Description of the Input File

The input parameters for the heat exchanger component needs explanantions.

```
[./ HX ]
 type = HeatExchanger
 eos = eos
 eos_secondary = eos
 position = '0 0 0'orientation = '1 0 0'
 A = 0.785398163e-4A_s = c_0 d_0 r = 0.785398163e-4
 Dh = 0.01
 Dh_secondary = 0.01
 length = 1
 n elems = 10
 Hw = 1. e4Hw_secondary = 1. e4
 Phf = 0.031415926520
 Phf_secondary = 0.031415926520
 f = 0.01f<sub>secondary</sub> = 0.01Twall\_init = 300.0dim_wall = 1
```

```
wall_thickness = 0.001
 material\_wall = wall-mat
 n_wall_elems = 2
[../]
```


5.10 Example 10: A Loop With Core Channel and Heat Exchanger

5.10.1 Problem Description

Figure 10. Diagram of a loop with core channel and heat exchanger

This example is a simple loop whcich consists of 6 pipes, a core channel, and a heat exchanger. Each component differs in length, but has the same area and diameter. The core channel is used to heat up the liquid, while the heat exchanger is used to cool it down. Pipe 5 is used to control the system pressure. The input parameters are listed in the following:

Materials: Fuel Thermal conductivity = 29.3 W/m K Specific heat = 191.67 J/kg K Density = 1.4583*e*4*kg*/*m* 3

Clad

Thermal conductivity = 26.3 W/m K Specific heat = 638 J/kg K Density = 7.646*e*3*kg*/*m* 3

Wall Thermal conductivity = 26.3 W/m K Specific heat = 638 J/kg K Density = 7.646*e*3*kg*/*m* 3

Reactor's initial power = 5.129e7

Pipe1: Area = $0.44934m^2$ Diameter = 2.972e-3 m Length $= 1$ m Friction Coefficient = 0.001 $Hw = 0.0$

Pipe 2 length $= 5.18$ m Pipe 3 length $= 1$ m Pipe 4 length $= 2.27$ m Pipe 5 length $= 0.02$ m Pipe 6 length $= 0.3$ m

Core Channel: Length = 0.8 m Friction coefficient $= 0.022$ Convective heat transfer coefficient = 1.6129e5 Heat flux perimeter $= 497.778$
Initial solid temperature $= 628.15 \text{ K}$ Width of each heat structure = 0.00348 0.00052'

Heat Exchanger: Area of primary pipe = $0.44934m^2$ Area of secondary pipe = $0.44934m^2$ Diameter of primary pipe = 0.0186 m Diameter of secondary pipe = 0.014 m Length = 3.71 m Primary convective heat transfer coefficient = 1.6129e5 Secondary convective heat transfer coefficient = 1.6129e5 Primary heat flux perimeter= 327.568 Secondary heat flux perimeter = 327.568 Friction coefficient = 0.022 Initial wall temperature $= 628.15 \text{ K}$ Dimension of mesh used for wall $= 1$ Thickness of the wall between primary and secondary loop $= 0.0044$ m

Branches: Form loss coefficients = $0.5 0.5$ ['] Area = $0.44934m^2$ Initial Pressure = 1e5 Pa (Branch $1 = 2e5$ Pa)

Inlet: Type = TimeDependentJunction Input = 'pipe 6 (in)' Velocity = 0.5 m/s Temperature = 628.15 K

Outlet 1: Type = TimeDependentVolume $Input = 'IHX$ (secondary_out)' Pressure $= 1.0e5$ Pa Temperature = 761.15 K

Outlet 2: Type = TimeDependentVolume Input = 'pipe 5 (out)' Pressure = 1e5 Pa Temperature = 783.15 K

5.10.2 Input File

```
[GlobalParams]
 model_type = 3
 global_init_P = 1.0e5
 global_init_V = 0.5
 global\_init_T = 628.15stabilization_type = 'NONE'
\Box[EoS]
 [./eos]
   type = NonIsothermalEquationOfState
   p_0 = 1e5rho_0 = 865.51a2 = 5.7837e6beta = 2.7524e-4cv = 1272.0e_0 = 7.9898e5
   T_0 = 628.15[\ldots][]
[Materials]
 [./fuel-mat]
   type = SolidMaterialProperties
   k = 29.3Cp = 191.67rho = 1.4583e4
  [\ldots][./clad-mat]
   type = SolidMaterialProperties
   k = 26.3Cp = 638rho = 7.646e3[\ldots]
```

```
[./wall-mat]
   type = SolidMaterialProperties
   k = 26.3rho = 7.646e3Cp = 638[\ldots][]
[Components]
 [./reactor]
   type = Reactor
   initial_power = 5.1296e7
 [\ldots][./pipe1]
   type = Pipe
   eos = eos
   position = '0 1 0'orientation = '0 -1 0'A = 0.44934Dh = 2.972e-3length = 1n_elems = 5
   f = 0.001Hw = 0.0[\ldots][./CH1]
   type = CoreChannel
   eos = eos
   position = '0 0 0'orientation = '0 0 1'
   A = 0.44934Dh = 2.972e-3length = 0.8n_elems = 10
   f = 0.022Hw = 1.6129e5Phf = 497.778852000000
```

```
dim_hs = 1name_of_hs = 'fuel clad'
 Ts_init = 628.15
 n heatstruct = 2fuel_type = cylinder
 width of hs = '0.00348 0.00052'
 elem_number_of_hs = '4 1'
 material_hs = 'fuel-mat clad-mat'
 #peak_power = '1.3366e8 0.'
 power_fraction = '1.0 0.0'
[\,\ldots\,][./pipe2]
 type = Pipe
 eos = eos
 position = '0 0 0.8'
 orientation = '0 0 1'
 A = 0.44934Dh = 2.972e-3length = 5.18n_elems = 5
 f = 0.001Hw = 0.0[\ldots][./pipe3]
 type = Pipe
 eos = eos
 position = '0 0 5.98'
 orientation = '0 1 0'
 A = 0.44934
 Dh = 2.972e-3length = 1
 n elems = 5
 f = 0.001Hw = 0.0[\ldots][./IHX]
 type = HeatExchanger
 eos = eos
```

```
eos_secondary = eos
 position = '0 1.0 5.98'
 orientation = '0 0 -1'A = 0.44934A_secondary = 0.44934Dh = 0.0186
 Dh_secondary = 0.014
 length = 3.71n_elems = 10
 Hw = 1.6129e5Hw\_secondary = 1.6129e5Phf = 327.568860000000
 Phf_secondary = 327.568860000000
  f = 0.022f_secondary = 0.022Twall_init = 628.15wall_thickness = 0.0044
 dim\_wall = 1material_wall = wall-mat
  n_wall_elems = 2
[\ldots][./pipe4]
 type = Pipe
 eos = eos
 position = '0 1.0 2.27'
 orientation = '0 0 -1'A = 0.44934Dh = 2.972e-3length = 2.27n_elems = 5
 f = 0.001Hw = 0.0[\ldots][./pipe5]
 type = Pipe
 eos = eos
 position = '0 0 5.98'
 orientation = '0 0 1'
 A = 0.44934
```

```
Dh = 2.972e-3
 length = 0.02n_elems = 2
 f = 10Hw = 0.0[\ldots][./Branch1]
 type = Branch
 inputs = 'pipe1(out)'
 outputs = 'CH1(in) 'K = '0.5 0.5'Area = 0.44934Initial_pressure = 2e5
 eos = eos
[\ldots][./Branch2]
 type = Branch
  inputs = 'CH1(out)'outputs = 'pipe2(in)'
 K = '0.5 0.5'Area = 0.44934
 Initial_pressure = 1.0e5
 eos = eos
[\ldots][./Branch3]
 type = Branch
 inputs = 'pipe2(out)'
 outputs = 'pipe3(in) pipe5(in)'
 K = '0.0 0.0 0.0'Area = 0.44934
 Initial_pressure = 1e5
 eos = eos
[\ldots][./Branch4]
 type = Branch
  inputs = 'pipe3(out)'
  outputs = 'IHX(primary_in)'
```

```
K = '0.1 0.1'Area = 0.44934
 Initial_pressure = 1e5
 eos = eos
[../]
[./Branch5]
 type = Branch
 inputs = 'IHX(primary_out)'
 outputs = 'pipe4(in)'
 K = '0.0 0.0'Area = 0.44934
 Initial_pressure = 1e5
 eos = eos
[../]
[./Branch6]
 type = Branch
 inputs = 'pipe4(out)'
 outputs = 'pipe1(in)'K = '0.0 0.0'Area = 0.44934Initial_pressure = 1e5
 eos = eos
[../]
[./pipe6]
 type = Pipe
 eos = eos
 position = '0 1.5 2.27'
 orientation = '0 -1 0'
 A = 0.44934Dh = 2.972e-3length = 0.3n_elems = 5
 f = 0.001Hw = 0.0[\ldots][./Branch7]
```

```
type = Branch
```

```
inputs = 'pipe6(out)'
    outputs = 'IHX(secondary_in)'
   K = '0.0 0.0'Area = 0.44934Initial_pressure = 1e5
    eos = eos
  [\ldots][./inlet_TDJ]
   type = TimeDependentJunction
    input = 'pipe6(in)'
   v_{bc} = 0.5T bc = 628.15eos = eos
  [\ldots][./outlet_TDV]
   type = TimeDependentVolume
    input = 'IHX(secondary_out)'
   p_{bc} = '1.0e5'T_bc = 761.15
   eos = eos
  [../]
  [./TDV_p]
   type = TimeDependentVolume
    input = 'pipe5(out)'
   p_bc = '1e5'T_bc = 783.15
   eos = eos
 [\ldots][]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
   solve_type = 'PJFNK'
 [\ldots][]
```

```
[Executioner]
 type = Transient
 scheme = 'implicit-euler'
 dt = 1e-2
 dtmin = 1e-10
 nl rel tol = 1e-8nl\_abs\_tol = 1e-8nl_max_its = 30
 l\_tol = 1e-6l_max_its = 300
 start_time = 0.0
 num_steps = 500
 end time = 10.
 petsc_options_iname = '-pc_type -mat_fd_type -mat_mffd_type -ksp_gmres_restart'
 petsc_options_value = ' lu ds ds 300'
 [./Quadrature]
    type = TRAP
    order = FIRST
 [../]
[]
[Outputs]
 [./out]
   type = Exodus
   use_displaced = true
   output_initial = true
   sequence = false
   append_displaced = true
 [\ldots][./console]
   type = Console
  perf_log = true
 [\ldots][]
```
5.11 Example 11: A Model Pressurized Water Reactor Problem

5.11.1 Problem Description

Figure 11. Diagram of a model pressurized water reactor problem

This example shows a simplified PWR plant model. It is made up of thress sections - Loop A, Loop B and a reator vessel model. The reactor vessel region contains three parallel core channels, a bypass flow channel, and an upper and lower plenum. The three core channels represent all the cooling channels and fuel rods in the high power region, average power region and low power region of the reactor core respectively. The upper and lower plenum are modeled with volume branches. The two loops have a Hot Leg, a Heat Exchanger and its secondary side pipes, the Cold Leg and a primary Pump. The heat exchanger secondary side pipes are modeled with subcooled water since the steam generator model is not available yet. Loop A contains a time dependent volume component that works as a pressurizer to help regulate the system pressure.

5.11.2 Input File

```
[GlobalParams]
 model_type = 3
 global_init_P = 15.17e6
 global_init_V = 1.
 global\_init_T = 564.15scaling_factor_var = '1.e-1 1.e-5 1.e-8'
 temperature_sf = 1e-2
 stabilization_type = 'SUPG'
[]
[EoS]
 [./eos]
   type = NonIsothermalEquationOfState
   p_0 = 15.17e6rho_0 = 738.350a2 = 1.e7beta = .46e-3cv = 5.832e3
   e 0 = 3290122.80T_0 = 564.15[\ldots]\lceil]
[Materials]
 [./fuel-mat]
   type = SolidMaterialProperties
   k = 3.65Cp = 288.734
    rho = 1.0412e2
 [\ldots][./gap-mat]
   type = SolidMaterialProperties
   k = 1.084498
   Cp = 1.0rho = 1.0[\cdot,\cdot/]
```

```
[./clad-mat]
    type = SolidMaterialProperties
   k = 16.48672Cp = 321.384rho = 6.6e1[\ldots][./clad3-mat]
    type = SolidMaterialProperties
   k = 16.48672Cp = 6.6e3rho = 6.6e1[\ldots][./wall-mat]
    type = SolidMaterialProperties
   k = 100.0rho = 100.0Cp = 100.0[\ldots]\lceil]
[Components]
 active = 'reactor
            CH1 CH2 CH3 bypass_pipe LowerPlenum UpperPlenum
            DownComer-A
            pipe1-HL-A pipe2-HL-A
            HX-A
            pipe1-CL-A pipe2-CL-A
            Pump-A
            pipe1-SC-A pipe2-SC-A
            MassFlowRateIn-SC-A PressureOutlet-SC-A
            Branch1-A Branch2-A Branch3-A Branch4-A Branch5-A Branch6-A
            pipe-to-Pressurizer Pressurizer
            DownComer-B
            pipe1-HL-B pipe2-HL-B
            HX-B
            pipe1-CL-B pipe2-CL-B
            Pump-B
            pipe1-SC-B pipe2-SC-B
```

```
MassFlowRateIn-SC-B PressureOutlet-SC-B
          Branch1-B Branch2-B Branch3-B Branch4-B Branch5-B Branch6-B
          \boldsymbol{r}[./reactor]
 type = Reactor
  initial_power = 2.77199979e9
[\ldots]#Vessel region components
[./CH1]
 type = CoreChannel
 eos = eos
 position = '0 -1.2 0'orientation = '0 0 1'
 A = 1.161864Dh = 0.01332254
 length = 3.6576n elems = 8
 f = 0.01Hw = 5.33e4Phf = 321.341084980423
 Ts_init = 564.15
 dim hs = 1n_heatstruct = 3
 name_of_hs = 'FUEL GAP CLAD'
  fuel_type = cylinder
  width of hs = '0.0046955 0.0000955 0.000673'
  elem_number_of_hs = '3 1 1'
 material_hs = 'fuel-mat gap-mat clad-mat'
  power_fraction = '3.33672612e-1 0 0'
[\ldots]\lceil./CH2]
 type = CoreChannel
 eos = eos
 position = '0 0 0'orientation = '0 0 1'
 A = 1.549152542Dh = 0.01332254
  length = 3.6576
```

```
n_elems = 8 #16
 f = 0.01Hw = 5.33e4Phf = 428.454929876871
 Ts init = 564.15dim_hs = 1n heatstruct = 3
 name_of_hs = 'FUEL GAP CLAD'
 fuel_type = cylinder
 width_of_hs = '0.0046955 0.0000955 0.000673'
 elem_number_of_hs = '3 1 1'
 material_hs = 'fuel-mat gap-mat clad-mat'
 power_fraction = '3.69921461e-1 0 0'
[../]
[./CH3]
 type = CoreChannel
 eos = eos
 position = '0 1.2 0'
 orientation = '0 0 1'
 A = 1.858983051
 Dh = 0.01332254
 length = 3.6576n_elems = 8
 f = 0.01Hw = 5.33e4# aw = 276.5737513
 Phf = 514.145916018189
 Ts init = 564.15dim_h s = 1n_heatstruct = 3
 name_of_hs = 'FUEL GAP CLAD'
 fuel_type = cylinder
 width of hs = '0.0046955 0.0000955 0.000673'
 elem_number_of_hs = '3 1 1'
 material_hs = 'fuel-mat gap-mat clad3-mat'
 #peak_power = '3.401687e8 0. 0.'
 power_fraction = '2.96405926e-1 0 0'
[\ldots]
```
[./bypass_pipe]

```
type = Pipe
 eos = eos
 position = '0 1.5 0'
 orientation = '0 0 1'
 A = 1.589571014Dh = 1.42264
 length = 3.6576n_elems = 5
 f = 0.001Hw = 0.0[\ldots][./LowerPlenum]
 type = Branch
 eos = eos
 inputs = 'DownComer-A(out) DownComer-B(out)'
 outputs = 'CH1(in) CH2(in) CH3(in) bypass_pipe(in)'
 K = '0.2 0.2 0.2 0.2 0.4 40.0'Area = 3.618573408Initial_pressure = 151.7e5
[\ldots][./UpperPlenum]
 type = Branch
 eos = eos
 inputs = 'CH1(out) CH2(out) CH3(out) bypass_pipe(out)'
 outputs = 'pipe1-HL-A(in) pipe1-HL-B(in)'
 K = '0.5 0.5 0.5 80.0 0.5 0.5'Area = 7.562307456Initial_pressure = 151.7e5
[\ldots]#Loop A components
[./DownComer-A]
 type = Pipe
 eos = eos
 position = '0 2.0 4.0'
 orientation = '0 \t0 -1'A = 3.6185734Dh = 1.74724302
 length = 4
```

```
n_elems = 3
 f = 0.001Hw = 0.[\,.\,.\,/][./pipe1-HL-A]
 type = Pipe
 eos = eos
 position = '0 0.5 4.0'
 orientation = '0 0 1'
 A = 7.562307456Dh = 3.103003207
 length = 4.n_elems = 3
 f = 0.001Hw = 0.0[\ldots][./pipe2-HL-A]
 type = Pipe
 eos = eos
 position = '0 0.5 8.0'
 orientation = '0 1 0'
 A = 2.624474Dh = 1.828
 length = 3.5n_elems = 3
 f = 0.001Hw = 0.0[\ldots][./pipe1-CL-A]
 type = Pipe
 eos = eos
 position = '0 3.0 4.0'
 orientation = '0 -1 0'
 A = 2.624474Dh = 1.828
 length = 1.
 n_elems = 3
  f = 0.001
```

```
Hw = 0.0[../]
[./pipe2-CL-A]
 type = Pipe
 eos = eos
 position = '0 4 4.0'
 orientation = '0 -1 0'A = 2.624474Dh = 1.828
 length = 0.8n_elems = 3
 f = 0.001Hw = 0.0[../]
[./pipe1-SC-A]
 type = Pipe
 eos = eos
 position = '0 5.2 4.0'
 orientation = '0 -1 0'A = 2.624474Dh = 1.828
 length = 1.
 n_elems = 3
  f = 0.001Hw = 0.0[\ldots][./pipe2-SC-A]
 type = Pipe
 eos = eos
 position = '0 4.2 8.0'
 orientation = '0 1 0'
 A = 2.624474Dh = 1.828
 length = 1.n_elems = 3
 f = 0.001Hw = 0.0[\ldots]
```

```
[./Branch1-A]
  type = Branch
  eos = eos
  inputs = 'pipe1-HL-A(out)'
  outputs = 'pipe2-HL-A(in) pipe-to-Pressurizer(in)'
 K = '0.5 0.7 80.'Area = 7.562307456Initial_pressure = 151.7e5
[\ldots][./Branch2-A]
 type = Branch
 eos = eos
 inputs = 'pipe1-CL-A(out)'
  outputs = 'DownComer-A(in)'
 K = '0.5 0.7'Area = 3.6185734
  Initial_pressure = 151.7e5
[\ldots][./Branch3-A]
 type = Branch
 eos = eos
 inputs = 'pipe2-HL-A(out)'
 outputs = 'HX-A(primary_in)'
 K = '0.5 0.7'Area = 2.624474Initial_pressure = 151.7e5
[\ldots][./Pump-A]
 type = IdealPump
 eos = eos
  inputs = 'pipe2-CL-A(out)'
  outputs = 'pipe1-CL-A(in)'
 Area = 2.624474mass_flow_rate = 8801.1
 Initial_pressure = 151.7e5
[\ldots]
```

```
[./HX-A]
 type = HeatExchanger
  eos = eos
 eos_secondary = eos
 position = '0 4. 8.'
 orientation = '0 0 -1'A = 5.A_secondary = 5.
 Dh = 0.01
 Dh_secondary = 0.01
 length = 4.n_elems = 10
 Hw = 1.e4Hw_secondary = 1.e4
 Phf = 2695.100000000000
 Phf_secondary = 2695.100000000000
  f = 0.01f_secondary = 0.01dim wall = 1Twall init = 564.15wall_thickness = 0.001
 n_wall_elems = 2
 material_wall = wall-mat
[\ldots][./Branch4-A]
 type = Branch
 eos = eos
 inputs = 'pipe1-SC-A(out)'
 outputs = 'HX-A(secondary_in)'
 K = '0.5 0.7'Area = 2.624474e2Initial_pressure = 151.7e5
[\,.\,.\,/][./Branch5-A]
 type = Branch
 eos = eos
  inputs = 'HX-A(secondary_out)'
  outputs = 'pipe2-SC-A(in)'
```

```
K = '0.5 0.7'
```

```
Area = 2.624474e2
 Initial_pressure = 151.7e5
[\ldots][./Branch6-A]
 type = Branch
 eos = eos
 inputs = 'HX-A(primary_out)'
 outputs = 'pipe2-CL-A(in)'
 K = '0.5 0.7'Area = 2.624474e2Initial_pressure = 151.7e5
[\,.\,.\,]/[./MassFlowRateIn-SC-A]
 type = TimeDependentJunction
 input = 'pipe1-SC-A(in)'
 v_{\text{loc}} = 4.542T bc = 537.15eos = eos
[\ldots][./PressureOutlet-SC-A]
 type = TimeDependentVolume
 input = 'pipe2-SC-A(out)'
 p_{bc} = '151.7e5'T_bc = 564.15eos = eos
[\,.\,.]#Loop B components
[./DownComer-B]
 type = Pipe
 eos = eos
 position = '0 -2.0 4.0'orientation = '0 \t0 -1'A = 3.6185734
 Dh = 1.74724302
 length = 4n_elems = 3
 f = 0.001
```

```
Hw = 0.[../]
[./pipe1-HL-B]
 type = Pipe
 eos = eos
 position = '0 -0.5 4.0'orientation = '0 0 1'
 A = 7.562307456Dh = 3.103003207
 length = 4.n_elems = 3
 f = 0.001Hw = 0.0[\ldots][./pipe2-HL-B]
 type = Pipe
 eos = eos
 position = '0 -0.5 8.0'orientation = '0 -1 0'A = 2.624474Dh = 1.828
 length = 3.5n_elems = 3
  f = 0.001Hw = 0.0[\ldots][./pipe1-CL-B]
 type = Pipe
 eos = eos
 position = '0 -3.0 4.0'orientation = '0 1 0'
 A = 2.624474Dh = 1.828
 length = 1.n_elems = 3
 f = 0.001Hw = 0.0[\ldots]
```

```
[./pipe2-CL-B]
  type = Pipe
 eos = eos
 position = '0 -4.0 4.0'
 orientation = '0 1 0'
 A = 2.624474Dh = 1.828
 length = 0.8n_elems = 3
 f = 0.001Hw = 0.0[\ldots][./pipe1-SC-B]
 type = Pipe
 eos = eos
 position = '0 -5.2 4.0'orientation = '0 1 0'
 A = 2.624474Dh = 1.828
 length = 1.
 n_elems = 3
 f = 0.001Hw = 0.0[\ldots][./pipe2-SC-B]
 type = Pipe
 eos = eos
 position = '0 -4.2 8.0'orientation = '0 -1 0'
 A = 2.624474Dh = 1.828length = 1.
 n_elems = 3
 f = 0.001Hw = 0.0[../]
[./Branch1-B]
```

```
type = Branch
  eos = eos
  inputs = 'pipe1-HL-B(out)'
  outputs = 'pipe2-HL-B(in)'
 K = '0.5 0.7'Area = 7.562307456Initial_pressure = 151.7e5
[\ldots][./Branch2-B]
 type = Branch
  eos = eos
 inputs = 'pipe1-CL-B(out)'
  outputs = 'DownComer-B(in)'
 K = '0.5 0.7'Area = 3.6185734
  Initial_pressure = 151.7e5
[\ldots][./Branch3-B]
 type = Branch
 eos = eos
  inputs = 'pipe2-HL-B(out)'
 outputs = 'HX-B(primary_in)'
 K = '0.5 0.7'Area = 2.624474Initial_pressure = 151.7e5
[\ldots][./Pump-B]
 type = IdealPump
 eos = eos
 inputs = 'pipe2-CL-B(out)'
  outputs = 'pipe1-CL-B(in)'
 Area = 2.624474mass_flow_rate = 8801.1
  Initial_pressure = 151.7e5
[\ldots][./HX-B]
```

```
type = HeatExchanger
```

```
eos = eos
 eos_secondary = eos
 position = '0 -4.8.'orientation = '0 0 -1'A = 5.A_secondary = 5.
 Dh = 0.01
 Dh_secondary = 0.01
 length = 4.n_elems = 10
 Hw = 1.e4Hw\_secondary = 1.e4Phf = 2695.100000000000Phf_secondary = 2695.100000000000
 f = 0.01f_secondary = 0.01dim_wall = 1
 Twall_init = 564.15wall thickness = 0.001
 material_wall = wall-mat
 n_wall_elems = 2
 disp_mode = -1.0[\ldots][./Branch4-B]
 type = Branch
 eos = eos
 inputs = 'pipe1-SC-B(out)'
 outputs = 'HX-B(secondary_in)'
 K = '0.5 0.7'Area = 2.624474e2Initial_pressure = 151.7e5
[\ldots][./Branch5-B]
 type = Branch
 eos = eos
 inputs = 'HX-B(secondary_out)'
 outputs = 'pipe2-SC-B(in)'
 K = '0.5 0.7'Area = 2.624474e2
```

```
Initial_pressure = 151.7e5
 [\ldots][./Branch6-B]
   type = Branch
   eos = eos
   inputs = 'HX-B(primary_out)'
   outputs = 'pipe2-CL-B(in)'
   K = '0.5 0.7'Area = 2.624474e2Initial_pressure = 151.7e5
 [\ldots][./MassFlowRateIn-SC-B]
   #type = TDM
   type = TimeDependentJunction
   input = 'pipe1-SC-B(in)'
# massflowrate_bc = 8801.1
   v bc = 4.542T_bc = 537.15
   eos = eos
 [\,.\,.\,/][./PressureOutlet-SC-B]
   type = TimeDependentVolume
   input = 'pipe2-SC-B(out)'
   p_{bc} = '151.7e5'T bc = 564.15eos = eos
 [\ldots]# Pressurizer
 [./pipe-to-Pressurizer]
   type = Pipe
   eos = eos
   position = '0 0.5 8.0'
   orientation = '0 0 1'
   A = 2.624474Dh = 1.828length = 0.5n_elems = 3
```

```
f = 10.Hw = 0.0[\,.\,.\,/][./Pressurizer]
    type = TimeDependentVolume
    input = 'pipe-to-Pressurizer(out)'
    p_bc = '151.7e5'
   T_{DC} = 564.15eos = eos
  [\,.\,.\,/]\lceil]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
    solve_type = 'PJFNK'
  [\ldots][]
[Executioner]
  type = Transient
  scheme = 'implicit-euler'
  #use this parameter to have a better initial guess from previous two time steps, therefo
  [./Predictor]
   type = SimplePredictor
    scale = 0.6[\ldots]dt = 0.1dtmin = 1e-7
  nl_rel_tol = 1e-9
  nl\_abs\_tol = 1e-8nl_max\_its = 30l\_tol = 1e-4l_max\_its = 300start_time = 0.0
  end_time = 50
```

```
num_steps = 250
 petsc_options_iname = '-mat_fd_type -mat_mffd_type -ksp_gmres_restart -pc_type'
 petsc_options_value = 'ds ds 300 lu'
  [./Quadrature]
    type = TRAP
    order = FIRST
 [\ldots][]
[Outputs]
  [./out]
   type = Exodus
   use_displaced = true
   output_initial = true
   sequence = false
   append_displaced = true
  [\ldots][./console]
   type = Console
   perf_log = true
 [\ldots][ ]
```
5.11.3 Description of the Input File

Most of the input parameters have been explained in the previous examples. Only a few need some explanations here.

```
[./ Pump -A]
 type = IdealPump
  eos = eos
  inputs = 'pipe2 - CL - A(out)'outputs = 'pipe1 -CL -A( in )'
 Area = 2.624474mass_flow_rate = 8801.1
  Initial_pressure = 151.7 e5
[\cdot,\cdot/]
```


```
[./ Predictor ]
 type = SimplePredictor
 scale = 0.6[\ldots]
```


5.12 Example 12: A Simplified Primary System Model of a Boiling Water Reactor

5.12.1 Problem Description

Figure 12. Diagram of a simplified primary system of a BWR model

This example is a simplified primary system of a boiling water reactor. The model consists of down comer, lower plenum, reactor core, upper plenum, separator dryer, steam dome, main steam line, feedwater line and the primary pump model. One core channel is used to represent the entire reactor core. The lower plenum, upper lenum and steam dome are modeled with volume branch models. External to the reactor vessel, the main steam line is connected to the steam dome. A time dependent volume is attached to the main steam line to provide the necessary boundary conditions for the steam flow. A feedwater line is connected to the downcomer model. A time dependent volume is attached to the feedwater line to provide the necessary boundary conditions for the feedwater. Notably missing from this simplified BWR model are the jet pumps and the recirculation loops that allow the operator to vary coolant flow rate through the core and change the reactor power. Instead, a pump model is used to represent the functions of the jet pumps and the recirculation loops.

5.12.2 Input File

```
[GlobalParams]
 model_type = 32
 global_init_P = 7.e6
 global_init_V = 3.
 global_init_T = 517.
 scaling_factor_var = '1e-3 1e-4 1e-8'
 temperature_sf = '1e-4'
 gravity = '0 0 -9.8'stabilization_type = 'LAPIDUS'
[]
[EoS]
  [./two_phase_eos]
    type = TwoPhaseStiffenedGasEOS
  [\ldots][./vapor_phase_eos]
    type = StiffenedGasEquationOfStateVapor
  [\ldots][./liquid_phase_eos]
    type = StiffenedGasEquationOfStateLiquid
  [\ldots][]
[Materials]
  [./fuel-mat]
    type = SolidMaterialProperties
   k = 3.7Cp = 3.e2
```

```
rho = 10.42e3
```

```
[\ldots][./gap-mat]
   type = SolidMaterialProperties
   k = 0.7Cp = 5e3rho = 1.0[\ldots][./clad-mat]
   type = SolidMaterialProperties
   k = 16Cp = 356.
   rho = 6.551400e3[\cdot,\cdot/][]
[Components]
 [./reactor]
   type = Reactor
    initial_power = 3293.0e6
 [\ldots][./ch1]
   type = CoreChannel
   eos = two_phase_eos
   position = '0 0.0 5.28'
   orientation = '0 0 1'
   A = 7.8Dh = 1.3597E - 02length = 3.66n_elems = 100
    f = 0.2 \pm 0.05Hw = 5.0e4Phf = 1836.8430600
    Ts init = 517.
    fuel_type = cylinder
    dim_hs = 1n_heatstruct = 3
   name_of_hs = 'FUEL GAP CLAD'
    width_of_hs = '6.057900e-3 1.524000e-4 9.398000e-4'
    elem_number_of_hs = '5 1 2'
   material_hs = 'fuel-mat gap-mat clad-mat'
```

```
power_fraction = '1.0 0.0 0.0'
 stabilization_type = 'NONE'
 model_type = 32
[\,.\,.\,/][./pipe6]
 type = Pipe
 position = '0.0 0.0 10.82'
 orientation = '0 0 1'
 A = 3.93Dh = 1.0length = 2.72n elems = 40
 f = 0.1eos = two_phase_eos
 model_type = 32
 stabilization_type = 'NONE'
[\ldots][./pipe7]
 type = Pipe
 position = '0.0 0.0 15.42'
 orientation = '0 0 1'
 A = 3.93Dh = 1.0length = 0.1n_elems = 5
 f = 0.1eos = vapor_phase_eos
 model_type = 3
[\ldots][./pipe8]
 type = Pipe
 position = '0.0 2.0 14.48'
 orientation = '0 1 0'
 A = 3.93Dh = 1.0length = 0.5n_elems = 5
  f = 0.1
```

```
eos = liquid_phase_eos
 model_type = 3
 stabilization_type = 'SUPG'
[\ldots][./pipe9]
  # main steam line coming out of dome
 type = Pipe
 position = '0.0 3 18.92'
 orientation = '0 1 0'
 A = 1.32Dh = 1.0length = 1.0n_elems = 5
 f = 0.1eos = vapor_phase_eos
 model_type = 3
[\ldots][./pipe10]
 type = Pipe
 #position = '0.0 5.0 10.51'
 position = '0.0 2.75 2.10'
 orientation = '0 \t 0 \t -1'A = 8.55Dh = 1.0#length = 6.42length = 0.5n_elems = 5
 f = 0.1eos = liquid_phase_eos
 model_type = 3
 stabilization_type = 'SUPG'
[\ldots][./pipe11]
 type = Pipe
 position = '0.0 2.75 1.60'
 orientation = '0 \t 0 \t -1'A = 8.55Dh = 1.0
```

```
length = 0.5n_elems = 5
  f = 0.1eos = liquid_phase_eos
  model_type = 3
  stabilization_type = 'SUPG'
[\ldots][./pipe14]
  # main steam line to MIV
  type = Pipe
  position = '0.0 4.0 18.92'
  orientation = '0 1 0'
  A = 1.32Dh = 1.0length = 1.0n_elems = 5
  f = 0.0eos = vapor_phase_eos
  model_type = 3
[\,.\,.][./MainIsolationValve]
  type = VolumeBranch
  eos = vapor_phase_eos
  center = '0.0 5.0 18.92'
  inputs = ' pipe14(out)'
  outputs = 'pipe_steam_turbine(in)'
  K = '0.0 0.0'volume = 1.32Area = 1.32initial_T = 517.0scale_factors = '1.0E-4 1.0E-8 1.0' # rho, rhoE
[\ldots][./pipe_steam_turbine]
  # main steam line to TDV
  type = Pipe
  position = '0.0 5 18.92'
  orientation = '0 1 0'
  A = 1.32
```

```
Dh = 1.0length = 1.0n_elems = 5
 f = 0.0eos = vapor_phase_eos
 model_type = 3
[\ldots][./Pump]
 type = Pump
 eos = liquid_phase_eos
 inputs = 'pipe10(out)'
 outputs = 'pipe11(in)'
 Area = 3.0Initial_pressure = 7.3e6
 #mass_flow_rate = 12915.0
 Head = 40.0K_reverse = '10. 10.'[\ldots][./SeparatorDryer]
 type = SeparatorDryer
 eos = two_phase_eos
 center = '0.0 0.0 14.48'
 inputs = 'pipe6(out)'
 outputs = 'pipe7(in) pipe8(in)'
 K = '1.0 \quad 1.0 \quad 5.0'volume = 19.30Area = 10.27initial_T = 517.0scale_factors = '1.0E-3 1.0E-8 1.0E-0'
[\ldots][./lowerplenum]
 type = VolumeBranch
 eos = two_phase_eos
 center = '0.0 0.0 2.64'
 inputs = 'pipe11(out)'
 outputs = 'ch1(in)'K = '1.0 20.0'volume = 61.48
```

```
Area = 11.64
 initial_T = 517.0scale_factors = '1.0E-3 1.0E-8 1.0E-0'
[\ldots][./upperplenum]
  type = VolumeBranch
 eos = two_phase_eos
 center = '0.0 0.0 9.88'
 inputs = 'ch1(out)'outputs = 'pipe6(in)'
 K = '3.0 1.0'volume = 26.99Area = 14.36initial_T = 517.0scale_factors = '1.0E-3 1.0E-8 1.0E-0'
[\,.\,.\,/][./Dome]
 type = VolumeBranch
 eos = vapor_phase_eos
 center = '0.0 0.0 18.92'
 inputs = 'pipe7(out)'
 outputs = 'pipe9(in)'
 K = '1.0 1.0'volume = 178.19
 Area = 26.19scale factors = '1.0E-3 1.0E-8 1.0E-0'
[\,.\,.][./DownComer]
 type = DownComer
  eos = liquid_phase_eos
  center = '0.0 2.75 9.81'
  inputs = 'pipe8(out) pipe_feedwater3(out)'
 outputs = 'pipe10(in)'
 K = '1.0 10.0 1.0'volume = 201.3Area = 15initial_level = 13.42
 initial_T = 517.0
```
```
dome_component = 'Dome'
 dome_eos = vapor_phase_eos
 scale_factors = '1.0E-4 1.0E-9 1.0E-0'
[\ldots][./SteamLineBranch]
 type = VolumeBranch
 eos = vapor_phase_eos
 center = '0.0 4.0 18.92'
 inputs = 'pipe9(out)'
 outputs = 'pipe14(in)'K = '0.0 0.0'volume = 2.64Area = 1.32initial_T = 517.0scale_factors = '1.0E-4 1.0E-8 1.0'
[\ldots][./pipe_feedwater1]
 #feedwater line from TDV
 type = Pipe
 position = '0.0 6.0 12.52' #'0.0 7.0 12.52'
 orientation = '0 -1 0'A = 1.32Dh = 1.0length = 1.0n_elems = 5
 f = 0.01 #1
 eos = liquid_phase_eos
 model_type = 3
 stabilization_type = 'SUPG'
[\ldots][./FeedWaterValve]
 type = Valve
 eos = liquid_phase_eos
 center = '0.0 5.0 12.52'
 inputs = 'pipe_feedwater1(out)'
 outputs = 'pipe_feedwater2(in)'
 K = '0.0 0.0'volume = 1.32
```

```
Area = 1.32initial_T = 517.0initial_status = open
 trigger_time = 1.0E5
 response_time = 1.1E5
 scale factors = '1.0E-4 1.0E-8'
[\ldots][./pipe_feedwater2]
  #feedwater line from feed water valve
 type = Pipe
 position = '0.0 5.0 12.52' #'0.0 7.0 12.52'
 orientation = '0 -1 0'A = 1.32Dh = 1.0length = 1.0n_elems = 5
 f = 0.01eos = liquid_phase_eos
 model_type = 3
 stabilization_type = 'SUPG'
[\ldots][./branch_feedwater_line]
 type = VolumeBranch
 eos = liquid_phase_eos
 center = '0.0 4.0 12.52'
 inputs = 'pipe_feedwater2(out)'
 outputs = 'pipe_feedwater3(in)'
 K = '0 0'volume = 1.32Area = 1.32initial_T = 517.0scale factors = '1.0E-4 1.0E-8 1.0'[\ldots][./pipe_feedwater3]
 #feedwater line to downcomer
 type = Pipe
 position = '0.0 4.0 12.52' #'0.0 6.0 12.52'
 orientation = '0 -1 0'
```

```
A = 1.32Dh = 1.0length = 1.0n elems = 5
    f = 0.01eos = liquid_phase_eos
   model_type = 3
    stabilization_type = 'SUPG'
  [../]
  [./inlet]
    type = TimeDependentVolume
    input = 'pipe_feedwater1(in)'
   p_bc = 7.1e6T_bc = 508.eos = liquid_phase_eos
 [\ldots][./outlet1]
   type = TimeDependentVolume
    input = 'pipe_steam_turbine(out)'
   p\_bc = 7.0e6T_bc = 517
   eos = vapor_phase_eos
   weak_bc = false
 [\ldots][]
[Preconditioning]
 [./SMP_PJFNK]
   type = SMP
   full = true
   solve_type = 'PJFNK'
 [\,.\,.][]
[Executioner]
 type = Transient
 dtmin = 1.e-7
```
[./TimeStepper]

```
type = SolutionTimeAdaptiveDT
   dt = 0.1[\ldots]petsc_options_iname = '-ksp_gmres_restart -pc_type'
 petsc_options_value = '30 lu'
 nl_rel_tol = 1e-8
 nl\_abs\_tol = 1e-6nl_max\_its = 151_{\text{tol}} = 1e-5l_max_its = 100
 start_time = 0.0
 end_time = 400num_steps = 500000
 [./Quadrature]
   type = TRAP
   order = FIRST
 [\ldots][]
[Outputs]
 [./out]
    type = Exodus
    use_displaced = true
   output_initial = true
    sequence = false
   append_displaced = true
   interval = 50
  [\ldots][./console]
   type = Console
   perf_log = true
 [\ldots][./checkpoint]
   type = Checkpoint
   num_files = 1
```
[../] $[$]

5.12.3 Description of the Input File

```
[./ SeparatorDryer ]
 type = SeparatorDryer
 eos = two_phase_eos
 center = '0.0 0.0 14.48 '
 inputs = 'pipe6 (out)'outputs = 'pipe7(in) pipe8(in)'
 K = '1.0 1.0 5.0'volume = 19.30Area = 10.27initial_T = 517.0scale_factors = '1.0E-3 1.0E-8 1.0E-0'[\ldots]
```


scale factors The scaling factors for the primary variables of the separator dryer component.

```
[./ DownComer ]
 type = DownComer
 eos = liquid_phase_eos
 center = '0.0 2.75 9.81'
 inputs = ' pipe8 ( out ) pipe_feedwater3 ( out )'
 outputs = 'pipe10 (in)'K = '1.0 10.0 1.0'volume = 201.3Area = 15initial_level = 13.42
 initial_T = 517.0dome_component = 'Dome '
 dome_eos = vapor_phase_eos
 scale_factors = '1.0E-4 1.0E-9 1.0E-0'[\ldots]
```
[./DownComer] Subblock for the down comer component.


```
[./ FeedWaterValve ]
 type = Valve
 eos = liquid_phase_eos
 center = '0.0 5.0 12.52 '
 inputs = ' pipe_feedwater1 ( out )'
 outputs = ' pipe_feedwater2 ( in )'
 K = '0.0 0.0'volume = 1.32Area = 1.32initial_T = 517.0initial_status = open
 trigger_time = 1.0 E5
 response_time = 1.1 E5
 scale_factors = '1.0E-4 1.0E-8'[\ldots]
```
[./FeedWater] Subblock for the valve component.


```
[./ checkpoint ]
  type = Checkpoint
 num_files = 1
[../]
```


References

- [1] D. A. Knoll and D. E. Keyes, "Jacobian-free Newton-Krylov methods: a survey of approaches and applications," *Journal of Computational Physics*, vol. 193, pp. 357–397, Jan. 2004. [http:](http://dx.doi.org/10.1016/j.jcp.2003.08.010) [//dx.doi.org/10.1016/j.jcp.2003.08.010](http://dx.doi.org/10.1016/j.jcp.2003.08.010).
- [2] P. N. Brown and A. C. Hindmarsh, "Matrix-free methods for stiff systems of ODEs," *SIAM J. Numer. Anal.*, vol. 23, pp. 610–638, June 1986. <http://www.jstor.org/stable/2157527>.
- [3] B. S. Kirk, J. W. Peterson, R. H. Stogner, and G. F. Carey, "libMesh: A C++ Library for Parallel Adaptive Mesh Refinement/Coarsening Simulations," *Engineering with Computers*, vol. 22, no. 3–4, pp. 237–254, 2006. <http://dx.doi.org/10.1007/s00366-006-0049-3>.
- [4] S. Balay, W. D. Gropp, L. Curfman-McInnes, and B. F. Smith, "Efficient management of parallelism in object oriented numerical software libraries," in *Modern Software Tools in Scientific Computing* (E. Arge, A. M. Bruaset, and H. P. Langtangen, eds.), pp. 163–202, Birkhäuser Press, 1997.
- [5] M. Heroux *et al.*, "An overview of Trilinos," Tech. Rep. SAND2003-2927, Sandia National Laboratories, 2003.
- [6] H. Zhang, L. Zou, D. Andrs, H. Zhao, and R. C. Martineau, "Point Kinetics Calculations with Fully Coupled Thermal Fluids Reactivity Feedback," in *International Conference on Mathematics, Computational Methods & Reactor Physics (M&C 2013)*, (Sun Valley, Idaho, USA), May 5–9, 2013.
- [7] L. Zou, J. Peterson, H. Zhao, H. Zhang, D. Andrs, and R. C. Martineau, "Solving Multi-Mesh Flow and Conjugate Heat Transfer Problems with RELAP-7," in *International Conference on Mathematics, Computational Methods & Reactor Physics (M&C 2013)*, (Sun Valley, Idaho, USA), May 5–9, 2013.
- [8] R. D. Falgout and U. M. Yang, "HYPRE: A Library of High Performance Preconditioners," in *International Conference on Computational Science*, pp. 632–641, 2002.

 $v1.28$

