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# **Plant Reload Optimization**

Framework Overview & Demonstration



# **Framework Overview**

### **Background: Why it is important?**



#### 2022 Nuclear Cost Summary (\$/MWh)\*

- Fuel takes ~17% of the total generating cost
  - Costs ~\$43M for a typical LWR fuel reload in a year

### Factors affecting Fuel Cost\*\*



- Traditional methods deciding core loading pattern and reload quantity are labor-intensive and time-consuming.
  - More than 10E+30 combinations for 17x17 PWR core

### Automated simulation-based fuel reloading optimization framework is needed.

Applicable to flexible operations, ATF, high burn-up and extended cycle reactor core design

\*\* International Atomic Energy Agency (2020). "Reload Design and Core Management in Operating Nuclear Power Plants." IAES-TECDOC-1898, IAEA.

### **Core Design Development Process**



### **Optimization of Reactor Core Design**

### Balance between economics and safety

- Optimize fuel batch for economic benefits
- Multiple "safety" parameters to be considered
- Flexible for computational tools

### Al-based optimization methodology

- Genetic Algorithm (GA)
  - Based on Darwin's theory of evolution
  - Select best results from potential solutions
  - Multi-objective optimization with Non-Dominated Sorting Genetic Algorithm II (NSGA II)
- Looking for wide applications
  - LEU+, ATF, HBU, power-uprate, flexible operation
  - Non-LWRs or advanced nuclear systems
  - Multi-physics/Uncertainty analysis



Source: A Visual Guide to Evolutionary Strategies. https://blog.otoro.net/2017/10/29/visual-evolutionstrategies.

# **Optimization of Reactor Core Design Genetic Algorithm (GA) Overview**

### GA mimics natural selection and evolution

- No need of derivatives calculation
- Solves non-linear and non-convex problems by random evolution
- Removes biased results
- Constrained and unconstrained
- Continuous and discrete variables

#### GA iterates groups of solutions

- Set initial list of solutions (neutronics, thermal-hydraulics, etc)
- · Evaluate and determine potential solutions
- Random select best solution by
  - Clone, cross-over, and mutation operations.



### NSGA-II is...

· Multi-objective, fast non-dominated sorting elite GA

### • Why NSGA-II?

- · Lower computational complexity than NSGA-I
- · Population diversity is guaranteed.
- One of the multi-objective evolutionary computation benchmark

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A multi-objective optimization problem can be written as

Minimize (or maximize) (f_1(x), f_2(x), ..., f_M(x))^T

Subject to

g_j(x) \ge (\text{or } \le) 0

h_k(x) = 0

x_i^{(L)} \le x_i \le x_i^{(U)}

- f_m(x) is m-th objective, where m = 1, 2, ..., M.

- g_j(x) is j-th inequality constraint, where j = 1, 2, ..., J

- h_k(x) is k-th equality constraint, where k = 1, 2, ..., K

- x = (x_1, x_2, ..., x_n)^T is a n-dimensional vector

- x_i^{(L)} and x_i^{(U)} are the lower and upper bounds on i-th variable
```





- Keep the best chromosomes from parent and offspring population
- Elitism does not allow an already found optimal solutions to be deleted.



- Assign rank to each chromosome using the dominance depth
- Non-dominated points belong to first rank.
- The non-dominated solutions from remainder are in second rank, and so on.

### Niching for the First Rank



- Niching gives preference to chromosomes that are not crowded.
- Crowding distance measures crowdedness of a chromosome w.r.t. its neighbors lying on the same front.
  - Crowding distance = a + b
  - a and b are normalized distances.
- Chromosomes from the first rank are selected based on niching.

### Plant ReLoad Optimization (PRLO) Project Overview



HCF: Hot channel factor

DBA: Design basis accident

PCT: Peak cladding temperature DNBR: Departure of nucleate boiling rate HTC: Heat transfer coefficient IH: Thermal-hydraulics RIP: Rod internal pressure FFRD: Fuel failure, relocation and dispersal

# Single Cycle Core Design Optimization

# Single Cycle / Single Objective Optimization for Core Design Case Study Introduction

### Settings

- PWR core with 157 fuel assemblies (FA)
- Quarter-core symmetry
- 6 FA designs  $\rightarrow$  design space = 7.1×10<sup>32</sup>
- 200 Population w/ 90 Iteration for GA

| Fuel type<br>ID     | 0    | 1    | 2          | 3    | 4          | 5         |
|---------------------|------|------|------------|------|------------|-----------|
| Enrichment<br>(wt%) | 2    | 2.5  | 2.5        | 3.2  | 3.2        | Reflector |
| Burnable<br>poison  | None | None | 16 Gd rods | None | 16 Gd rods | -         |



### Objective

• Maximize cycle length (cycle energy production)

### Constraints

- F<sub>Q</sub> (Heat flux hot channel factor) < 2.1
- $F_{\Delta H}$  (Nuclear enthalpy rise hot channel factor) < 1.48
- Peak critical boron concentration (CBC) <1300 pcm

# Single Cycle / Single Objective Optimization for Core Design Demonstration



A generic PWR reactor core is used for the demonstration

# Single Cycle / Single Objective Optimization for Core Design Demonstration



A generic PWR reactor core is used for the demonstration

# Single Cycle / Multi Objective Optimization for Core Design Case Study Introduction

### Settings

- PWR core with 157 fuel assemblies (FA)
- Quarter-core symmetry
- 6 FA designs  $\rightarrow$  design space = 7.1×10<sup>32</sup>
- 100 Population w/ 50 Iteration for GA

| Fuel type<br>ID     | 1         | 2    | 3    | 4             | 5    | 6             |
|---------------------|-----------|------|------|---------------|------|---------------|
| Enrichment<br>(wt%) | Reflector | 2    | 2.5  | 2.5           | 3.2  | 3.2           |
| Burnable<br>poison  | -         | None | None | 16 Gd<br>rods | None | 16 Gd<br>rods |

### Objectives

- Maximize cycle length (cycle energy production)
- Minimize fuel cost

### Constraints

- F<sub>Q</sub> (Heat flux hot channel factor) < 2.1
- $F_{\Delta H}$  (Nuclear enthalpy rise hot channel factor) < 1.48
- Peak critical boron concentration (CBC) <1300 pcm

NOTE: F<sub>Q</sub> and F<sub>ΔH</sub> are peaking factors used to characterize core power distribution in terms of ratios of local maximum power output to average core output.

A generic PWR reactor core is used for the demonstration



Reflector

3.2 wt % No BP



# Single Cycle / Multi Objective Optimization for Core Design Demonstration



A generic PWR reactor core is used for the demonstration

# Single Cycle / Multi Objective Optimization for Core Design Demonstration



A generic PWR reactor core is used for the demonstration

## Single Cycle / Multi Objective Optin Demonstration





A generic PWR reactor core

### **Optimization Acceleration Technique**

### Adaptive Mutation / Crossover Probabilities



#### **Demonstration with ZDT1 Test**

Population size of 10 and 30 iterations



#### Population size of 50 and 30 iterations



| Method                | Number of<br>Iteration | Elapsed time<br>(sec) | Mean Squared<br>Error (%) |
|-----------------------|------------------------|-----------------------|---------------------------|
| Static                | 300                    | 846 sec               | 0.001%                    |
| Adaptive<br>(DHM/ILC) | 15                     | 13.89 sec             | 0.0001%                   |

# Cycle by Cycle Core Design Optimization

# Introduction of Cycle–by–Cycle Optimization Process Process Overview

 Cycle *n* optimization is linked to Cycle *n*+1 optimization through the Inventory Management step.



### Introduction of Cycle–by–Cycle Optimization Process System Code Interface with RAVEN



# Introduction of Cycle–by–Cycle Optimization Process AP1000 Reference Model

|    | R    | Р    | N    | M    | L    | K    | J    | н               | G               | F               | E               | D               | С               | в               | Α              |
|----|------|------|------|------|------|------|------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------------|
| 1  |      |      |      |      |      |      | J-01 | H-01            | G-01            |                 |                 |                 |                 |                 |                |
| 2  |      |      |      |      | L-02 | K-02 | J-02 | H-02            | G-02            | F-02            | E-02            |                 |                 |                 |                |
| 3  |      |      |      | M-03 | L-03 | K-03 | J-03 | H-03            | G-03            | F-03            | E-03            | D-03            |                 |                 |                |
| 4  |      |      | N-04 | M-04 | L-04 | K-04 | J-04 | H-04            | G-04            | F-04            | E-04            | D-04            | C-04            |                 |                |
| 5  |      | P-05 | N-05 | M-05 | L-05 | K-05 | J-05 | H-05            | G-05            | F-05            | E-05            | D-05            | C-05            | B-05            |                |
| 6  |      | P-06 | N-06 | M-06 | L-06 | K-06 | J-06 | H-06            | G-06            | F-06            | E-06            | D-06            | C-06            | B-06            |                |
| 7  | R-07 | P-07 | N-07 | M-07 | L-07 | K-07 | J-07 | H-07            | G-07            | F-07            | E-07            | D-07            | C-07            | B-07            | A-07           |
| 8  | R-08 | P-08 | N-08 | M-08 | L-08 | K-08 | J-08 | H-08<br>ID = 1  | G-08            | F-08            | E-08            | D-08            | C-08            | B-08            | A-08           |
| 9  | R-09 | P-09 | N-09 | M-09 | L-09 | к-09 | J-09 | H-09<br>ID = 2  | G-09<br>ID = 3  | F-09<br>ID = 4  | E-09<br>ID = 5  | D-09<br>ID = 6  | C-09<br>ID = 7  | B-09<br>ID = 8  | A-09<br>ID = 9 |
| 10 |      | P-10 | N-10 | M-10 | L-10 | K-10 | J-10 | H-10<br>ID = 10 | G-10<br>ID = 11 | F-10<br>ID = 12 | E-10<br>ID = 13 | D-10<br>ID = 14 | C-10<br>ID = 15 | B-10<br>ID = 16 |                |
| 11 |      | P-11 | N-11 | M-11 | L-11 | K-11 | J-11 | H-11<br>ID = 17 | G-11<br>ID = 18 | F-11<br>ID = 19 | E-11<br>ID = 20 | D-11<br>ID = 21 | C-11<br>ID = 22 | B-11<br>ID = 23 |                |
| 12 |      |      | N-12 | M-12 | L-12 | K-12 | J-12 | H-12<br>ID = 24 | G-12<br>ID = 25 | F-12<br>ID = 26 | E-12<br>ID = 27 | D-12<br>ID = 28 | C-12<br>ID = 29 |                 |                |
| 13 |      |      |      | M-13 | L-13 | К-13 | J-13 | H-13<br>ID = 30 | G-13<br>ID = 31 | F-13<br>ID = 32 | E-13<br>ID = 33 | D-13<br>ID = 34 |                 |                 |                |
| 14 |      |      |      |      | L-14 | K-14 | J-14 | H-14<br>ID = 35 | G-14<br>ID = 36 | F-14<br>ID = 37 | E-14<br>ID = 38 |                 | -               |                 |                |
| 15 |      |      |      |      |      |      | J-15 | H-15<br>ID = 39 | G-15<br>ID = 40 |                 |                 | -               |                 |                 |                |

Label map for a generic AP1000 reactor using quarter symmetrical perturbations

|    | R    | Р    | N    | М    | L    | к    | J    | н             | G             | F             | E             | D             | С             | в             | Α            |
|----|------|------|------|------|------|------|------|---------------|---------------|---------------|---------------|---------------|---------------|---------------|--------------|
| 1  |      |      |      |      |      |      | J-01 | H-01          | G-01          |               |               |               |               |               |              |
| 2  | ]    |      |      |      | L-02 | K-02 | J-02 | H-02          | G-02          | F-02          | E-02          |               |               |               |              |
| 3  |      |      |      | M-03 | L-03 | K-03 | J-03 | H-03          | G-03          | F-03          | E-03          | D-03          |               | _             |              |
| 4  |      |      | N-04 | M-04 | L-04 | K-04 | J-04 | H-04          | G-04          | F-04          | E-04          | D-04          | C-04          |               |              |
| 5  |      | P-05 | N-05 | M-05 | L-05 | K-05 | J-05 | H-05          | G-05          | F-05          | E-15          | D-05          | C-05          | B-05          |              |
| 6  |      | P-06 | N-06 | M-06 | L-06 | K-06 | J-06 | H-06          | G-06          | F-06          | E-06          | D-06          | C-06          | B-06          |              |
| 7  | R-07 | P-07 | N-07 | M-07 | L-07 | K-07 | J-07 | H-07          | G-07          | F-07          | E-07          | D-07          | C-07          | B-07          | A-07         |
| 8  | R-08 | P-08 | N-08 | M-08 | L-08 | K-08 | J-08 | H-08<br>ID=0  | G-08          | F-08          | E-08          | D-08          | C-08          | B-08          | A-08         |
| 9  | R-09 | P-09 | N-09 | M-09 | L-09 | K-09 | J-09 | H-09<br>ID=1  | G-09<br>ID=2  | F-09<br>ID=3  | E-09<br>ID=4  | D-09<br>ID=5  | C-09<br>ID=6  | B-09<br>ID=7  | A-09<br>ID=8 |
| 10 |      | P-10 | N-10 | M-10 | L-10 | K-10 | J-10 | C-12<br>ID=9  | G-10<br>ID=10 | F-10<br>ID=11 | E-10<br>ID=12 | D-10<br>ID=13 | C-10<br>ID=14 | B-10<br>ID=15 |              |
| 11 |      | P-11 | N-11 | M-11 | L 11 | K-11 | J-11 | H-11<br>ID=16 | G-11<br>ID=17 | F-41<br>ID=18 | E-11<br>ID=19 | D-11<br>ID=20 | C-11<br>ID=21 | B-11<br>ID=22 |              |
| 12 |      |      | N-12 | M-12 | L-12 | K-12 | J-12 | H-12<br>ID=23 | G-12<br>ID=24 | F-12<br>ID=25 | E-12<br>ID=26 | D-12<br>ID=27 | H-10<br>ID=28 |               |              |
| 13 |      |      |      | M-13 | L-13 | K-13 | J-13 | H-13<br>ID=29 | G-13<br>ID=30 | F-13<br>ID=31 | E-13<br>ID=32 | D-13<br>ID=33 |               |               |              |
| 14 |      |      |      |      | L-14 | K-14 | J-14 | H-14<br>ID=34 | G-14<br>ID=35 | F-14<br>ID=36 | E-14<br>ID=37 |               |               |               |              |
| 15 |      |      |      |      |      |      | J-15 | H-15<br>ID=38 | G-15<br>ID=39 |               |               |               |               |               |              |

Example of a location perturbation using quarter-core symmetry, resulting in simultaneous permutation of the symmetrical counterparts in the other quadrants.

## Introduction of Cycle–by–Cycle Optimization Process Reference Solution



#### Key performance parameters

| Variable                           | Value  |
|------------------------------------|--------|
| Cycle Length (EFPD)                | 353.2  |
| Critical Boron Concentration (ppm) | 1457.2 |
| F <sub>Q</sub>                     | 1.901  |
| F <sub>ΔH</sub>                    | 1.552  |

BOC exposure map in GWd/MT for the reference case of the generic AP1000 equilibrium cycle model.

# **Comparison of Objective Target: Genetic Algorithm Optimization**

### Case A: Maximize Cycle Length

| 37.996       | 31.212       | 16.402       | 16.234       | 24.974       | 14.471  | 25.989 | ( |
|--------------|--------------|--------------|--------------|--------------|---------|--------|---|
| 3B           | 2B           | 1B           | 1B           | 2B           | 1B      | 2B     | F |
| 31.212       | 0            | 30.86        | 25.95        | 12.352       | 29.388  | 0      | F |
| 2B           | FF           | 2B           | 2B           | 1B           | 2B      | FF     |   |
| 16.402       | 30.071       | 10.446       | 14.714       | 25.677       | 10.565  | 0      |   |
| 1B           | 2B           | 1B           | 1B           | 2B           | 1B      | FF     |   |
| 16.234       | 10.43        | 17.034       | 28.95        | 10.683       | 16.672  | 0      |   |
| 1B           | 1B           | 1B           | 2B           | 1B           | 1B      | FF     |   |
| 24.974<br>2B | 10.795<br>1B | 25.752<br>2B | 25.478<br>2B | 10.359<br>1B | 0<br>FF |        |   |
| 14.471<br>1B | 31.79<br>2B  | 27.053<br>2B | 0<br>FF      | 0<br>FF      |         |        |   |
| 25.989<br>2B | 0<br>FF      | 0<br>FF      | 0<br>FF      |              |         |        |   |
| 0<br>FF      | 0<br>FF      |              |              |              |         |        |   |

#### Case B: Maximize Core-averaged Burnup

| 37.996       | 10.359       | 10.43        | 30.86        | 17.034  | 16.234  | 25.989 | 0  |
|--------------|--------------|--------------|--------------|---------|---------|--------|----|
| 3B           | 1B           | 1B           | 2B           | 1B      | 1B      | 2B     | FF |
| 10.359       | 24.974       | 25.478       | 10.565       | 16.672  | 14.471  | 12.352 | 0  |
| 1B           | 2B           | 2B           | 1B           | 1B      | 1B      | 1B     | FF |
| 10.43        | 25.677       | 16.402       | 25.752       | 14.714  | 25.95   | 0      |    |
| 1B           | 2B           | 1B           | 2B           | 1B      | 2B      | FF     |    |
| 30.86        | 29.388       | 0            | 31.212       | 30.071  | 0       | 0      |    |
| 2B           | 2B           | FF           | 2B           | 2B      | FF      | FF     |    |
| 17.034<br>1B | 10.446<br>1B | 31.79<br>2B  | 27.053<br>2B | 0<br>FF | 0<br>FF |        |    |
| 16.234<br>1B | 28.95<br>2B  | 10.795<br>1B | 10.683<br>1B | 0<br>FF |         |        |    |
| 25.989<br>2B | 0<br>FF      | 0<br>FF      | 0<br>FF      |         |         |        |    |
| 0<br>FF      | 0<br>FF      |              |              |         |         |        |    |

| Variable                  | Reference | Case A  | Case B  |
|---------------------------|-----------|---------|---------|
| Cycle Length (EFPD)       | 353.2     | 353.5   | 353.5   |
| Boron Concentration (ppm) | 1457.20   | 1456.94 | 1456.90 |
| F <sub>Q</sub>            | 1.901     | 1.781   | 1.775   |
| $F_{\Delta H}$            | 1.552     | 1.463   | 1.458   |

# **Comparison of Objective Target: Genetic Algorithm Convergence**

Case A: Maximize Cycle Length



#### Case B: Maximize Core-averaged Burnup



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# Example of Fuel Inventory Management: Case A – Cycle n & Cycle n+1

#### Cycle n

| 48.476<br>3B |              |              |              |              |             |    |              |              | _        |
|--------------|--------------|--------------|--------------|--------------|-------------|----|--------------|--------------|----------|
| 43.451<br>2B | 17.036<br>FF | 43.602<br>2B | 39.139<br>2B | 27.49<br>1B  | 42.6<br>2B  | 79 | 16.758<br>FF | 10.388<br>FF |          |
| 30.814<br>1B | 43.437<br>2B | 26.332<br>1B | 29.617<br>1B | 39.283<br>2B | 26.23<br>1B | 27 | 14.271<br>FF |              |          |
| 31.193<br>1B | 26.835<br>1B | 31.753<br>1B | 41.552<br>2B | 25.817<br>1B | 29.8<br>1B  | 21 | 9.838<br>FF  |              | BU [GWd/ |
| 38.781<br>2B | 26.512<br>1B | 38.57<br>2B  | 38.137<br>2B | 24.252<br>1B | 10.53<br>FF | 24 |              |              |          |
| 29.198<br>1B | 44.058<br>2B | 39.561<br>2B | 15.728<br>FF | 11.041<br>FF |             |    |              |              |          |
| 39.223<br>2B | 16.058<br>FF | 13.61<br>FF  | 10.238<br>FF |              | [           | Bu |              | Nd/t1        |          |
| 12.112<br>FF | 10.159<br>FF |              |              |              |             | bu | Batch        | ina, g       |          |

H-08 D-09 C-09 A-09 H-09 G-09 F-09 E-09 B-09 H-10 G-10 F-10 E-10 D-10 C-10 B-10 H-11 G-11 F-11 E-11 D-11 C-11 B-11 F-12 G-12 E-12 D-12 C-12 H-12 F-13 G-13 E-13 H-13 D-13 **Removed Fuel** G-14 F-14 E-14 H-14 Assemblies **Recycled Fuel** H-15 G-15 Assemblies

Cycle n+1

The most burned fuel assemblies are removed, and fresh fuel assemblies are temporarily placed in the positions of the discarded spent fuel.

## **Cycle-by-Cycle Optimization Results**

#### Cycle n

| 48.476<br>3B |              |              |              |              |              |              |              |       |
|--------------|--------------|--------------|--------------|--------------|--------------|--------------|--------------|-------|
| 43.451<br>2B | 17.036<br>FF | 43.602<br>2B | 39.139<br>2B | 27.49<br>1B  | 42.679<br>2B | 16.758<br>FF | 10.388<br>FF |       |
| 30.814<br>1B | 43.437<br>2B | 26.332<br>1B | 29.617<br>1B | 39.283<br>2B | 26.227<br>1B | 14.271<br>FF |              |       |
| 31.193<br>1B | 26.835<br>1B | 31.753<br>1B | 41.552<br>2B | 25.817<br>1B | 29.821<br>1B | 9.838<br>FF  | BU [GW       | /d/t] |
| 38.781<br>2B | 26.512<br>1B | 38.57<br>2B  | 38.137<br>2B | 24.252<br>1B | 10.524<br>FF |              |              |       |
| 29.198<br>1B | 44.058<br>2B | 39.561<br>2B | 15.728<br>FF | 11.041<br>FF |              |              |              |       |
| 39.223<br>2B | 16.058<br>FF | 13.61<br>FF  | 10.238<br>FF |              |              | 1011111      | 1            |       |
| 12.112<br>FF | 10.159<br>FF |              |              |              | Burnup<br>Ba | tch          |              |       |





| Variable                  | Reference | <i>n</i> ycle 10 | <i>n</i> +1:le 11 |
|---------------------------|-----------|------------------|-------------------|
| Cycle Length (EFPD)       | 353.2     | 353.5            | 353.3             |
| Boron Concentration (ppm) | 1457.2    | 1456.9           | 1456.8            |
|                           | 1.90      | 1.78             | 1.83              |
|                           | 1.55      | 1.46             | 1.49              |

# Accomplishment & Future Plan

# Plant ReLoad Optimization (PRLO) Project Major Accomplishments

- Development of GA-based optimization platform
  - Single and multi-objective optimizer
  - Fuel Inventory Management Interface
  - Multi-cycle (Cycle-by-Cycle) optimization
- Computational tools coupling and testing
  - RAVEN is a base platform
  - PARCS, SIMULATE, RELAP5-3D, TRANSURANUS
- Demonstration in Multiphysics optimization problem
  - Core design / safety analysis / fuel performance
- Development and demonstration of multi-physics uncertainty analysis capability with RELAP5-3D
  - Focus on reflood phenomena in LBLOCA
- Stakeholder engagement Industrial Partner
  - Benchmark test ongoing with historical data from NPP of Constellation Energy.



# Plant ReLoad Optimization (PRLO) Project Technology Roadmap

|                           | Phase 1 (FY 19 – 20)<br>Development of<br>Methodology | Phase 2 (FY 21 – 22)<br>Improvement of<br>Planform for PWR | Phase 3 (FY 22 – 23)<br>Completion of<br>Planform for PWR | Phase 4 (FY 24 – 25)<br>Demonstration and<br>Expansion for PWR                |
|---------------------------|---|--|---|---|
| Multi–Physics<br>Analysis | Set plant-based scenarios                             | Apply risk-informed approach                               | Analyze uncertainties from<br>multi – physics             |   |
|                           | Simulate DBA<br>with deterministic method             |  |   |   |
|                           | Use fixed core loading pattern                        |  |   |   |
|                           | Evaluate recoverable margin                           |  |   |   |
| Platform<br>Development   | Setup tools & methods                                 | Assess constraints & issues of code interface              | Investigate optimization acceleration methods             | Apply optimization acceleration methods                                       |
|                           |   | Investigate optimization algorithms for fuel reloading     | Integrate of multi–objective optimization algorithm       | Enhance platform capability for multi–cycle optimization                      |
| Demonstration             |   |  | Demonstrate single-cycle<br>optimization of a genetic PWR | Demonstrate multi–cycle<br>optimization of a genetic PWR                      |
|                           |   |  |   | Demonstrate PWR core<br>optimization performance in<br>comparison to industry |
| Stakeholder<br>Engagement |   |  | Initiate industrial partnership                           | Extend industrial partnership for PWR core optimization                       |

# **Any Questions?**





# **APPENDIX**

### "Cycle-by-Cycle" Optimization Process in the PRLO Framework

